

LS-DYNA EXAMPLES MANUAL

March 1998

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Introduction

This is an assembly of example problems provided by a number of resources. The resources and histories are documented in the acknowledgment and reference sections. Users are encouraged to submit examples which will facilitate the education of LS-DYNA users.

October 1997 Modifications

- All examples were documented and re-organized for clarity.
- All examples ran successfully using LS-DYNA version 940 on a Sun SPARC 10 workstation.
- Many examples required changes to make them work. Descriptions of the examples were updated to reflect the examples as they are as of this date.
- All graphics in this edition have been replaced with newly created results using LS-TAURUS on the Sun SPARC 10 workstation.
- Many new examples were added to the manual.
- The examples are now strictly in keyword format. References to ingrid and structured format have been removed for they are no longer consistent with these examples.
- Naming Conventions for the examples have been changed as described below.

Naming Convention

The naming convention for the input decks is: keyword.description.k Keyword defines the major keyword used within the example. Description defines either the action or the physical content of the problem. The “.k” on the end of the filename signifies that the file is a keyword format LS-DYNA input file.

INTRODUCTION

LS-DYNA Manual Section: *AIRBAG_SIMPLE_AIRBAG_MODEL

Additional Sections:

*CONTACT_NODES_TO_SURFACE
*RIGIDWALL_PLANAR

Example: Airbag Deploys into Cylinder

Filename: airbag.deploy.k

Description:

An airbag inflates below a rigid cylinder, causing the cylinder to fly into the air.

Model:

The volume pressure relationships is defined by the Simple Airbag Model for control volumes. The bag inflates through the flow of mass into the bag.

Input:

The control volume defines the thermodynamic relationship for the gas in terms of parameters such as heat capacity, gas temperature, incoming mass, and outgoing mass (*AIRBAG_SIMPLE_AIRBAG_MODEL). A rigidwall is used below the airbag to act as ground (*RIGIDWALL_PLANAR). A ground is displayed using rigid shell elements, but is used only for visualization purposes. The contact between the airbag and the cylinder is automatically generated by part id (*CONTACT_NODES_TO_SURFACE).

Results:

The plots show the bag expanding. The ASCII file abstat contains information on the computed pressure, volume, mass flow and internal energy of the control volume (*DATABASE_ABSTAT).

***AIRBAG_SIMPLE_AIRBAG_MODEL**
Airbag Deploys into Cylinder

```
$
*DATABASE_RCFORC
$   dt
  2.000E-04
$
*DATABASE_RBDOUT
$   dt
  2.000E-04
$
*DATABASE_RWFORC
$   dt
  2.000E-04
$
$$$$ Airbag
$
$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*AIRBAG_SIMPLE_AIRBAG_MODEL
$   sid   sidtyp   rbid   vsca   psca   vini   mwd   spsf
$     1     1
$
$   cv     cp     t     lcid     mu     a     pe     ro
$ 1.736E+03 2.430E+03 1.200E+03     1 7.000E-01 0.000E+00 1.470E+01 3.821E-06
$
$   lou
$
$
*SET_PART_LIST
$   sid   da1     da2     da3     da4
$     1
$
$   pid1   pid2     pid3     pid4     pid5     pid6     pid7     pid8
$     3
$
*DEFINE_CURVE
$   lcid   sidr     scla     sclo     offa     offo
$     1
$
$         abscissa      ordinate
$         0.000E+00      0.000E+00
$         3.200E-02      2.600E+01
$         4.500E-02      6.000E-01
$         8.000E-02      1.000E-01
$
$$$$
$
$$$$ Rigid Walls
$
$$$$
$
$$$$ Ground
$
*RIGIDWALL_PLANAR
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$   nsid   nsidex   boxid
$     0     0       0
$
$   xt     yt     zt     xh     yh     zh     fric
$     0.0   0.0   0.0   0.0   1.0   0.0   0.5
$
```


***AIRBAG_SIMPLE_AIRBAG_MODEL**

Airbag Deploys into Cylinder

6993	1	7547	7509	7148	7549
6994	1	7509	7510	7149	7148
6995	1	7510	7511	7150	7149

.
... in total, 3792 shells defined

6990	3	7078	7048	7144	7145
6991	3	7108	7078	7145	7146
6992	3	5998	7108	7146	7147

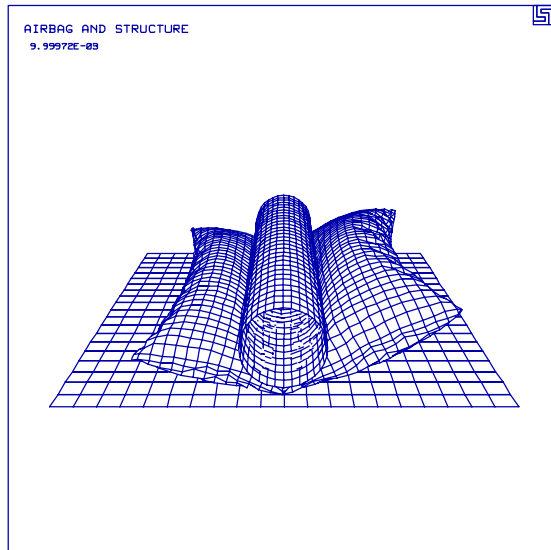
\$
*END

*AIRBAG_SIMPLE_AIRBAG_MODEL

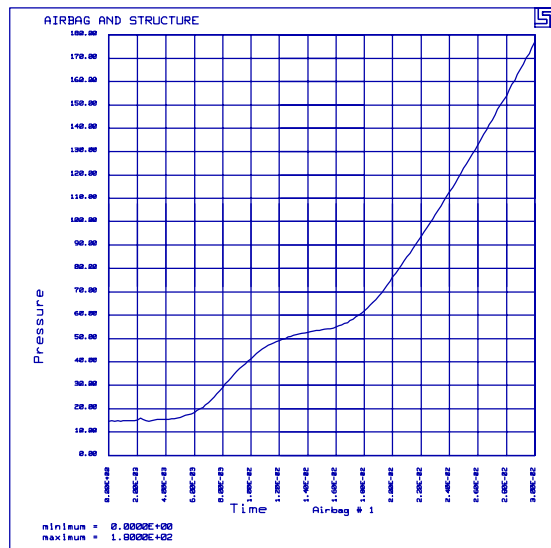
Airbag Deploys into Cylinder

Results:

taurus g=d3plot
19
state 15 rx 20 view



phs3
abstat
grid oset 0
180 pressure



***AIRBAG_SIMPLE_AIRBAG_MODEL**
Airbag Deploys into Cylinder

LS-DYNA Manual Section: *BOUNDARY_PRESCRIBED_MOTION

Additional Sections:

*LOAD_SEGMENT

Example: Blow Molding

Filename: boundary_prescribed_motion.blow-mold.k

Description:

This problem includes two tools, a punch nose and a die tube. A blank tube is formed by blow molding the nose through the tube.

Model:

The hollow tube blank is made with 600 shell elements AND has an outer radius of 12.06 mm, an initial thickness of 1.37 mm, and an initial length of 53.5 mm. The internal pressure of the hollow tube blank is 40 N/mm^2 applied using the *LOAD_SEGMENT keyword. The tools are rigid shell elements. Only 1/4 of the system is modeled because of symmetry.

The motion of the punch nose and the end of the blank follow a linear motion with a total displacement of 15 mm (*BOUNDARY_PRESCRIBED_MOTION).

Reference:

Wei, Lixin

*BOUNDARY_PRESCRIBED_MOTION

Blow Molding

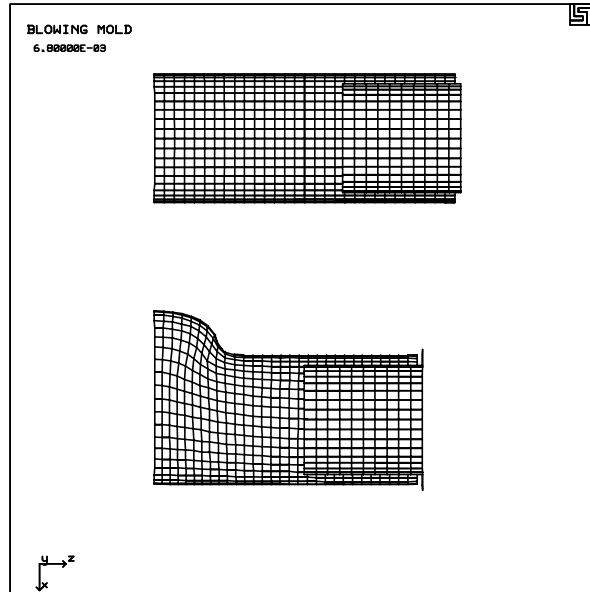
```
*NODE
$   nid          x          y          z          tc          rc
   1001  .130103000E+02  -.113825400E+01  .535000000E+02
   1002  .129937800E+02  .126376400E+01  .535000000E+02
   .
   ... in total, 1437 nodes defined
   .
   3650  -.113750000E+02  .442958800E-05  .517166600E+02
   3651  -.113750000E+02  .442958800E-05  .534999900E+02
$
$$$$$$$$$ Shell Elements
$
*ELEMENT_SHELL
$   eid      pid      n1      n2      n3      n4
   1001      1      1001      1002      1003      1004
   1002      1      1004      1003      1005      1006
   .
   ... in total, 1313 shells defined
   .
   2197      2      2226      2187      2198      2227
   2198      2      2227      2198      2209      2228
$
*END
```

*BOUNDARY_PRESCRIBED_MOTION

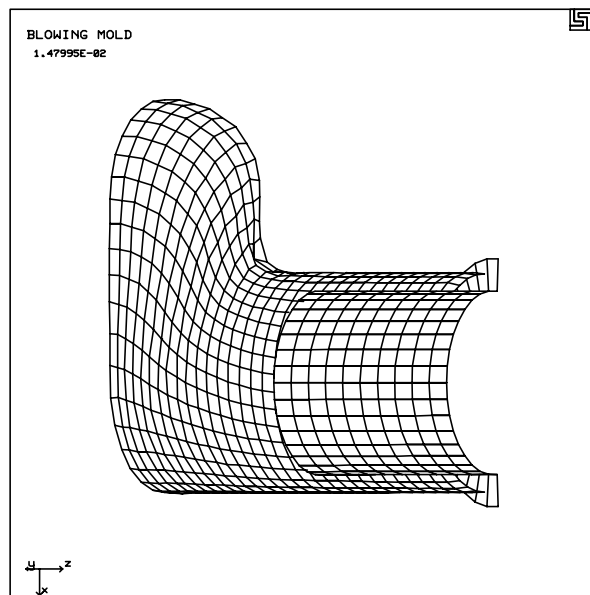
Blow Molding

Results:

taurus g=d3plot
angle 1 rz -90 ry 90 -m 1 dist 6000
ytrans 40 view ytrans -50 s 35 over view



s 75
ry 30
center view



***BOUNDARY_PRESCRIBED_MOTION**
Blow Molding

***CONSTRAINED_GENERALIZED_WELD**
Two Plates Connected With Butt Welds

LS-DYNA Manual Section: *CONSTRAINED_GENERALIZED_WELD

Additional Sections:

*DATABASE_CROSS_SECTION_PLANE

Example: Two Plates Connected with Butt Welds

Filename: constrained.butt-weld.k

Description:

Two plates are connected by four butt welds. The plates are pulled apart and the center two welds fail.

Model:

Each plate is constructed with 12 shell elements. One end of one plate is fixed with SPC's. One end of the other plate has a prescribed motion condition defined. The other ends of the plates are butt welded together with failure criteria. Cross sections are defined through each plate to monitor the forces through the plates as they are pulled apart.

Results:

```
butt weld constraint failed between nodes      35 & 23
: Time          = 1.26913E+00 : xl-force   = 5.56053E+00
: yl-force     = 2.28915E-03 : zl-force   = -1.93680E-07
: xl-moment    = -3.16675E-07 : yl-moment  = 9.09511E-07
: plastic ep=  0.00000E+00
```

Stresses in weld:

```
: signn       = 2.78026E-01 : tautn      = 0.00000E+00
: signm       = 9.09511E-08 : tautm      = 0.00000E+00
: signs       = 0.00000E+00 : tauts      = 1.14458E-04
: tautw       = -9.68398E-09
```

```
butt weld constraint failed between nodes      37 & 25
: Time          = 1.26913E+00 : xl-force   = 5.56054E+00
: yl-force     = -2.29328E-03 : zl-force   = -2.41027E-07
: xl-moment    = 2.97763E-07 : yl-moment  = 3.22515E-07
: plastic ep=  0.00000E+00
```

Stresses in weld:

```
: signn       = 2.78027E-01 : tautn      = 0.00000E+00
: signm       = 3.22515E-08 : tautm      = 0.00000E+00
: signs       = 0.00000E+00 : tauts      = -1.14664E-04
: tautw       = -1.20514E-08
```


*CONSTRAINED_GENERALIZED_WELD

Two Plates Connected With Butt Welds

```
0.1
$
*DATABASE_HISTORY_NODE
$   id1      id2      id3      id4
    22       23       35       36
$
*DATABASE_SECFORC
$   dt
    0.010
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Define Cross Sections
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*DATABASE_CROSS_SECTION_PLANE
$   psid      xct      yct      zct      xch      ych      zch
    0         15.0     0.0      0.0      100.0    0.0     0.0
$   xhev      yhev      xhev      lenl     lenm
    15.0      1.0      0.0
$
$
*DATABASE_CROSS_SECTION_PLANE
$   psid      xct      yct      zct      xch      ych      zch
    0         65.0     0.0      0.0      100.0    0.0     0.0
$   xhev      yhev      xhev      lenl     lenm
    65.0      1.0      0.0
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Constrain the Plates Together with 4 Butt welds
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
$$$$$$$ weld 1
$
*CONSTRAINED_GENERALIZED_WELD_BUTT
$   nsid      cid
    21
$
$   tfail      epsf      sigy      beta      L      D      Lt
    0.3        0.250    0.9      10.0     2.0     1.0
$
*SET_NODE_LIST
$   sid
    21
$   nid1      nid2
    21       33
$
$
$$$$$$$ weld 2
$
*CONSTRAINED_GENERALIZED_WELD_BUTT
$   nsid      cid
    23
$
$   tfail      epsf      sigy      beta      L      D      Lt
    0.3        0.250    0.9      10.0     2.0     1.0
```

*CONSTRAINED_GENERALIZED_WELD

Two Plates Connected With Butt Welds

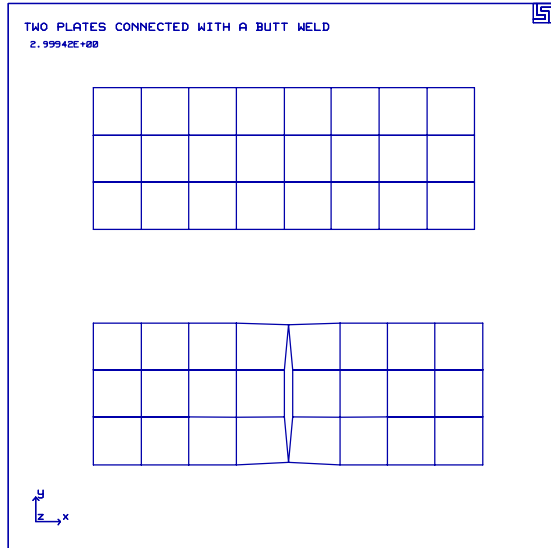
```
1 5.000000000E+01 2.000000000E+01 0.000000000E+00
2 6.000000000E+01 2.000000000E+01 0.000000000E+00
.
... in total, 40 nodes defined
.
39 4.000000000E+01 0.000000000E+00 0.000000000E+00
40 8.000000000E+01 0.000000000E+00 0.000000000E+00
$
$$$$$$$$ Shell Elements
$
*ELEMENT_SHELL
$  eid      pid      n1      n2      n3      n4
   1         2       20       14        8       22
   2         2       14       15        9        8
.
... in total, 24 shells defined
.
23         3         5         6       32       31
24         3         6        38       40       32
$
*END
```

*CONSTRAINED_GENERALIZED_WELD

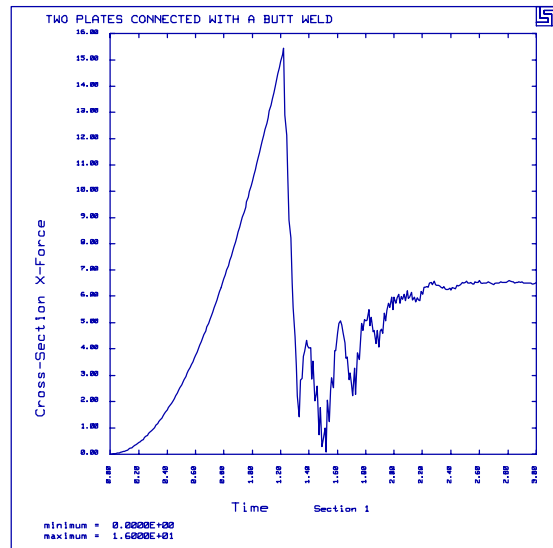
Two Plates Connected With Butt Welds

Results:

taurus g=d3plot
ytran 25 view
ytran -50 state 16 over view



phs3
secforc
smooth 5
oset 0 16 x-for 1



***CONSTRAINED_GENERALIZED_WELD**

Two Plates Connected With Butt Welds

LS-DYNA Manual Section: *CONSTRAINED_JOINT_PLANAR

Additional Sections:

*LOAD_NODE_POINT
*LOAD_SEGMENT
*INITIAL_VELOCITY_NODE
*CONSTRAINED_EXTRA_NODES_SET

Example: Sliding Blocks with Planar Joint

Filename: constrained.joint_planar.k

Description:

This problem illustrates a planar joint connecting two rigid bodies.

Model:

The first block measuring $2 \times 2 \times 2$ slides along a second block measuring $2 \times 2 \times 8$. A third flexible body controls the time step size. The first block has a ramped pressure of 100 psi applied to the top surface and ramped concentrated forces applied to a lower edge of 40 lbs. The initial velocity of the first block is 400 inches/second.

Input:

One joint definition consist of nodes 128, 126, 129 and 127 (*CONSTRAINED_JOINT_PLANAR). The nodes are extra nodes attached to the rigid bodies and are coincident (*CONSTRAINED_EXTRA_NODES_SET, *SET_NODE_LIST).

Results:

The plots show that the first block correctly slides across the second block.

*CONSTRAINED_JOINT_PLANAR

Sliding Blocks with Planar Joint

List of LS-DYNA input deck:

```
*KEYWORD
*TITLE
test planar joints
$
$   LSTC Example
$
$   Last Modified: August 29, 1997
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$   - part 1: fixed, long, rigid block
$   - part 2: rigid block which slides on top of part 1
$             initial velocity = 400
$   - part 3: elastic solid used to set time step
$
$
$   Units: lbf-s^2/in, in, s, lbf, psi, lbf-in
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Control Output
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONTROL_TERMINATION
$   endtim   endcyc   dtmin   endneg   endmas
$         0.020
$
*DATABASE_BINARY_D3PLOT
$   dt/cycl   lcdt
$         0.001
$
*DATABASE_GLSTAT
$   dt
$     0.0001
$
*DATABASE_JNTFORC
$   dt
$     0.0001
$
*DATABASE_HISTORY_NODE
$   Define nodes that output into nodout
$   id1      id2      id3      id4      id5      id6      id7      id8
$       91       21       94      128      126      129      127
$
*DATABASE_NODOUT
$   dt
$     0.0001
$
*DATABASE_RBDOUT
$   dt
$     0.0001
$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Planar Joint
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
```

*CONSTRAINED_JOINT_PLANAR Sliding Blocks with Planar Joint

```

$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONSTRAINED_JOINT_PLANAR
$
$      n1      n2      n3      n4      n5      n6      rps
$      128      126      129      127      127      0.000E+00
$
*CONSTRAINED_EXTRA_NODES_SET
$
$      pid      nsid
$      1         1
$
*SET_NODE_LIST
$
$      sid
$      1
$
$      nid1      nid2      nid3      nid4      nid5      nid6      nid7      nid8
$      126        127
$
*CONSTRAINED_EXTRA_NODES_SET
$
$      pid      nsid
$      2         2
$
*SET_NODE_LIST
$
$      sid
$      2
$
$      nid1      nid2      nid3      nid4      nid5      nid6      nid7      nid8
$      128        129
$
$$$$$ Parts and Materials
$
$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*PART
fixed rigid body
$
$      pid      sid      mid      eosid      hgid      igrav      adpopt
$      1         1         1
$
*PART
sliding rigid body
$
$      2         2         2
$
*PART
elastic body for time step control
$
$      3         3         3
$
$$$$$ Materials
$
*MAT_RIGID
$
$      mid      ro      e      pr      n      couple      m      alias
$      1 7.850E-04 3.000E+07 3.000E-01

```

*CONSTRAINED_JOINT_PLANAR

Sliding Blocks with Planar Joint

```
$
$   cmo     con1     con2
$  1.000E+00 7.000E+00 7.000E+00
$
$  lco/a1     a2     a3     v1     v2     v3
$
$
$*MAT_RIGID
$
$   mid     ro     e     pr     n     couple     m     alias
$     2 7.850E-04 3.000E+07 3.000E-01
$
$   cmo     con1     con2
$
$  lco/a1     a2     a3     v1     v2     v3
$
$
$*MAT_ELASTIC
$
$   mid     ro     e     pr
$     3 7.850E-04 3.000E+07 3.000E-01
$
$
$$$$ Sections
$
$*SECTION_SOLID
$   sid  elform
$     1      0
$     2      0
$     3      0
$
$$$$
$$$$ Loading
$$$$
$$$$ Pressure load on top of block
$
$*LOAD_SEGMENT
$
$   lcid     sf     at     n1     n2     n3     n4
$     1 1.000E+00 0.000E+00     97     106     107     98
$     1 1.000E+00 0.000E+00    106     115     116     107
$     1 1.000E+00 0.000E+00     98     107     108     99
$     1 1.000E+00 0.000E+00    107     116     117     108
$
$*DEFINE_CURVE
$
$   lcid     sidr     scla     sclo     offa     offo
$     1         0 0.000E+00 0.000E+00 0.000E+00 0.000E+00
$
$   abscissa     ordinate
$  0.00000000E+00  0.00000000E+00
$  9.99999978E-03  1.00000000E+02
$  1.99999996E-02  1.00000000E+02
$
$
$$$$ Force load on lower edge of block
$
$*LOAD_NODE_POINT
$
```

***CONSTRAINED_JOINT_PLANAR**
Sliding Blocks with Planar Joint

```

$      nid      dof      lcld      sf      cid      m1      m2      m3
      91         3         2-1.000E+00      0
      92         3         2-1.000E+00      0
      93         3         2-1.000E+00      0
$
*DEFINE_CURVE
$
$      lcld      sidr      scla      sclo      offa      offo
      2          0 0.000E+00 0.000E+00 0.000E+00 0.000E+00
$
$      abscissa      ordinate
      0.00000000E+00      0.00000000E+00
      1.99999999E-02      4.00000000E+01
$$
$
$$$$ Initial Conditions
$
$$$$
$
*INITIAL_VELOCITY_NODE
$
$      nid      vx      vy      vz      vxe      vye      vze
$
$$$ Nodes on sliding block
$
      91 4.000E+02 0.000E+00 0.000E+00
      92 4.000E+02 0.000E+00 0.000E+00
      93 4.000E+02 0.000E+00 0.000E+00
      94 4.000E+02 0.000E+00 0.000E+00
      95 4.000E+02 0.000E+00 0.000E+00
      96 4.000E+02 0.000E+00 0.000E+00
      97 4.000E+02 0.000E+00 0.000E+00
      98 4.000E+02 0.000E+00 0.000E+00
      99 4.000E+02 0.000E+00 0.000E+00
     100 4.000E+02 0.000E+00 0.000E+00
     101 4.000E+02 0.000E+00 0.000E+00
     102 4.000E+02 0.000E+00 0.000E+00
     103 4.000E+02 0.000E+00 0.000E+00
     104 4.000E+02 0.000E+00 0.000E+00
     105 4.000E+02 0.000E+00 0.000E+00
     106 4.000E+02 0.000E+00 0.000E+00
     107 4.000E+02 0.000E+00 0.000E+00
     108 4.000E+02 0.000E+00 0.000E+00
     109 4.000E+02 0.000E+00 0.000E+00
     110 4.000E+02 0.000E+00 0.000E+00
     111 4.000E+02 0.000E+00 0.000E+00
     112 4.000E+02 0.000E+00 0.000E+00
     113 4.000E+02 0.000E+00 0.000E+00
     114 4.000E+02 0.000E+00 0.000E+00
     115 4.000E+02 0.000E+00 0.000E+00
     116 4.000E+02 0.000E+00 0.000E+00
     117 4.000E+02 0.000E+00 0.000E+00
$
$$$ Extra nodes on sliding rigid block
$
      128 4.000E+02 0.000E+00 0.000E+00
      129 4.000E+02 0.000E+00 0.000E+00
$
$$$$
$

```

*CONSTRAINED_JOINT_PLANAR

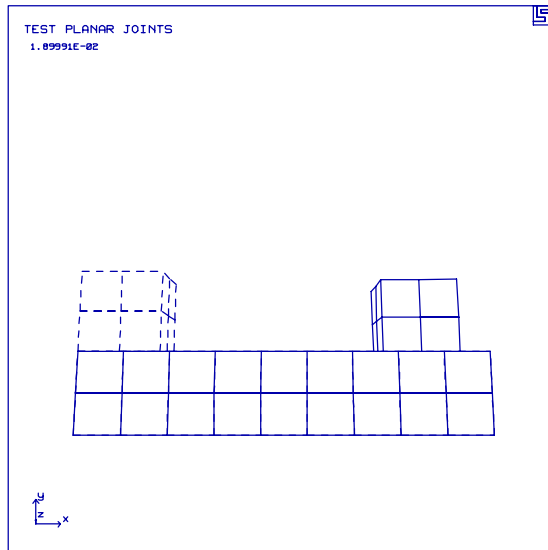
Sliding Blocks with Planar Joint

Results:

taurus g=d3plot

19

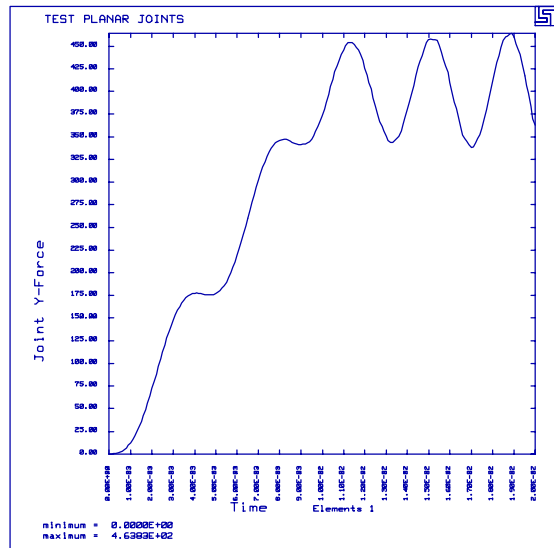
<m 3 rx -10 udg 1 state 20 over view



phs3

jntforc

oscl -1 y-force



***CONSTRAINED_JOINT_PLANAR**
Sliding Blocks with Planar Joint

*CONSTRAINED_JOINT_REVOLUTE Hinged Shell with Stop Angle (Revolute Joint)

LS-DYNA Manual Section: *CONSTRAINED_JOINT_REVOLUTE

Additional Sections:

*CONSTRAINED_JOINT_STIFFNESS
*CONTROL_TIMESTEP

Example: Hinged Shell with Stop Angle (Revolute Joint)

Filename: constrained_joint_revolute.k

Description:

Two rigid shell elements are joined together using a revolute joint. A stop angle is defined so that the rotating plate can only rotate 30 degrees relative to the other plate.

Model:

A pair of concentrated loads are applied to the end nodes of a hinge-jointed shell system using *LOAD_NODE_POINT. One of the rigid plates is fixed by using the capability within the *MAT_RIGID keyword. The rotating plate has a stop angle of 30 degrees relative to the fixed plate defined using the *CONSTRAINED_JOINT_STIFFNESS_GENERALIZED keyword.

Because all components in the model are rigid, the time step needs to be controlled by limiting the maximum time step to 4.15E-06 s. (In deformable structures, the minimum time step is usually the one of concern.)

Results:

The rotating plate at several states are shown imposed on each other. The maximum rotated angle is closer to 38 degrees rather than the specified 30 degrees. This is because the joint stiffness actual defines the angle at which the resistance force is to begin. The forces associated with stopping the rotating plate can be determined by examining the jntforc ascii file.

***CONSTRAINED_JOINT_REVOLUTE**
Hinged Shell with Stop Angle (Revolute Joint)

List of LS-DYNA input deck:

```

*KEYWORD
*TITLE
hinged shell w/ stop angle
$
$  LSTC Example
$
$  Last Modified: October 16, 1997
$
$ - This problem has a pair of concentrated loads applied to
$  the end nodes of a hinge-jointed shell system.
$
$ - 30 degree stop angle (must add joint stiffness, local coord system)
$
$ - control timestep with maximum 4.15E-06
$
$  Units: lbf-s2/in, in, s, lbf, psi, lbf-in
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1.>...2.>...3.>...4.>...5.>...6.>...7.>...8
$
*CONTROL_TERMINATION
$  endtim  endcyc  dtmin  endeng  endmas
  2.000E-02
$
*CONTROL_TIMESTEP
$  dtinit  scft  isdo  tslimt  dtms  lctm  erode  mslst
                               5
$
*DEFINE_CURVE
$  lcid  sidr  scla  sclo  offa  offo
   5
$      abscissa  ordinate
           0.0      4.15E-06
           1.0      4.15E-06
$
*DATABASE_BINARY_D3PLOT
$  dt  lcdt
  5.000E-04
$
*DATABASE_GLSTAT
$  dt
  0.0001
$
*DATABASE_JNTFORC
$  dt
  1.000E-04
$
*DATABASE_NODOUT
$  dt
  0.0001
$
*DATABASE_HISTORY_NODE
$  nid1  nid2
   3    4
$

```

***CONSTRAINED_JOINT_REVOLUTE**
Hinged Shell with Stop Angle (Revolute Joint)

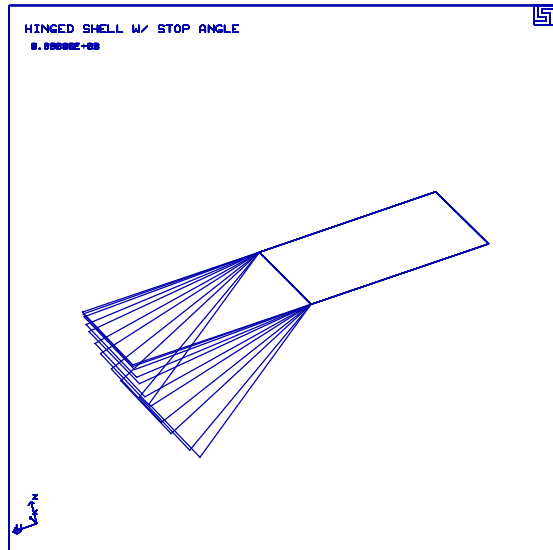
```
*DATABASE_RBDOUT
$ dt
  0.0001
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$ Revolute Joint
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONSTRAINED_JOINT_REVOLUTE
$
$ Create a revolute joint between two rigid bodies. The rigid bodies must
$ share a common edge to define the joint along. This edge, however, must
$ not have the nodes merged together. Rigid bodies A and B will rotate
$ relative to each other along the axis defined by the common edge.
$
$ Nodes 1 and 2 are on rigid body A and coincide with nodes 9 and 10
$ on rigid body B, respectively. (This defines the axis of rotation.)
$
$ The relative penalty stiffness on the revolute joint is to be 1.0,
$ the joint is well lubricated, thus no damping at the joint is supplied.
$
$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$ n1 n2 n3 n4 n5 n6 rps damp
$ 1 9 2 10 1.0
$
$
$$$$$$$$$$$$ Define a joint stiffness for the revolute joint described above.
$
$ Attributes of the joint stiffness:
$ - Used for defining a stop angle of 30 degrees rotation
$ (i.e., the joint allows a positive rotation of 30 degrees and
$ then imparts an elastic stiffness to prevent further rotation)
$ - Define between rigid body A (part 1) and rigid body B (part 2)
$ - Define a local coordinate system along the revolute axis
$ on rigid body A - nodes 1, 2 and 3 (cid = 5). This is used to
$ define the revolute angles phi (PH), theta (T), and psi (PS).
$ - The elastic stiffness per unit radian for the stop angles
$ are 100, 10, 10 for PH, T, and PS, respectively.
$ - Values not specified are not used during the simulation.
$
$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONSTRAINED_JOINT_STIFFNESS_GENERALIZED
$ jsid pidA pidB cidA cidB
$ 1 1 2 5 5
$
$ lcidPH lcidT lcidPS dlcidPH dlcidT dlcidPS
$
$ esPH fmPS esT fmT esPS fmPS
$ 100.0 10.0
$
$ nsAPH psaPH nsAT psaT nsAPS psaPS
$ 30.0
$
$
*DEFINE_COORDINATE_NODES
$ cid n1 n2 n3
```

*CONSTRAINED_JOINT_REVOLUTE

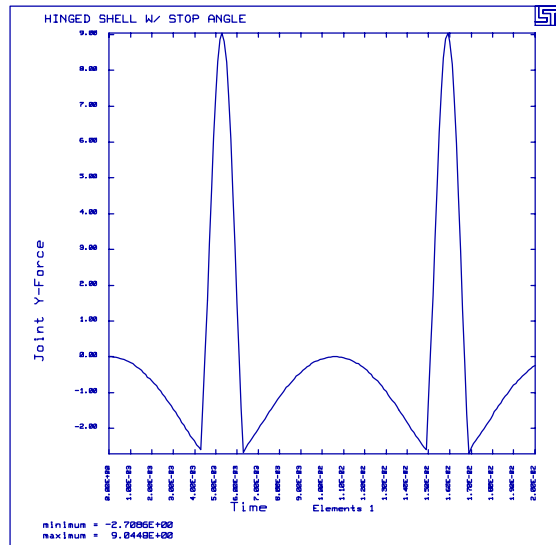
Hinged Shell with Stop Angle (Revolute Joint)

Results:

taurus g=d3plot
angle 1 rz 90 rx -45 ry 30 rx -15 rz 30 ry -20 s 1 v s 3 over v
s 5 over v ...repeat for all odd states up to ... s 21 over v



phs3
jntforc
y-force



LS-DYNA Manual Section: *CONSTRAINED_LINEAR

Additional Sections:

BOUNDARY_PRESCRIBED_MOTION_NODE
DEFINE_CURVE

Example: Linearly Constrained Plate

Filename: constrained.linear.plate.k

Description:

The center node of a plate moves in the normal direction. Two other nodes that are neighbors to the center node are constrained such that their displacement in the normal direction is identical.

Model:

The plate is made of an elastic material measuring $40 \times 40 \times 2 \text{ mm}^3$ and contains 64 Hughes-Liu shell elements. The center node displacement increases linearly. At the termination time, 0.0005 seconds, the displacement is 15 mm. The degree of freedom in the z-direction for the two nodes is identical.

Input:

A load curve defines the magnitude of the prescribed displacement of the center node (*BOUNDARY_PRESCRIBED_MOTION_NODE, *DEFINE_CURVE). A linear constraint card defines the coupling of the displacement in the z-direction between the two nodes (*CONSTRAINED_LINEAR). Two equal coefficients with opposite signs control the displacement.

Reference:

Schweizerhof, K. and Weimer, K.

***CONSTRAINED_LINEAR**
Linearly Constrained Plate

```

$      dt
    0.00001
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Constraints and Boundary Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>....1.>....2.>....3.>....4.>....5.>....6.>....7.>....8
$
$$$$ nodes 40 and 42 are constrained to have identical z-direction motion
$
*CONSTRAINED_LINEAR
$      num
    2
$
$      nid      dofx      dofy      dofz      dofrx      dofry      dofzr      coef
    40              1
    42              1      -1.00
$
$
$$$$ node 41 is displaced in the z-direction according to load curve 1
$
*BOUNDARY_PRESCRIBED_MOTION_NODE
$      nid      dof      vad      lcid      sf      vid
    41          3          2          1      1.0
$
*DEFINE_CURVE
$      lcid      sidr      scla      sclo      offa      offo
    1
$
$      abscissa      ordinate
          0.0          0.0
          0.0005      -15.0
          0.0015      -15.1
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
*PART
Impacted Material
$      pid      sid      mid      eosid      hgid      adpopt
    1          1          1          0          0          0
$
$
$$$$$$$ Materials
$
*MAT_ELASTIC
$      mid      ro      e      pr      da      db      k
    1      2.00e-8 100000.0 0.300
$
$
$$$$$$$ Sections
$
*SECTION_SHELL
$      sid      elform      shrf      nip      propt      qr/irid      icomp
    1          6      0.83333      2.0      3.0
$
$      t1      t2      t3      t4      nloc

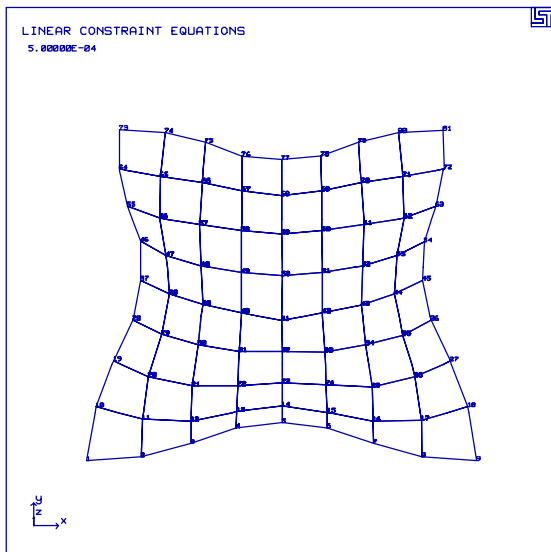
```

*CONSTRAINED_LINEAR

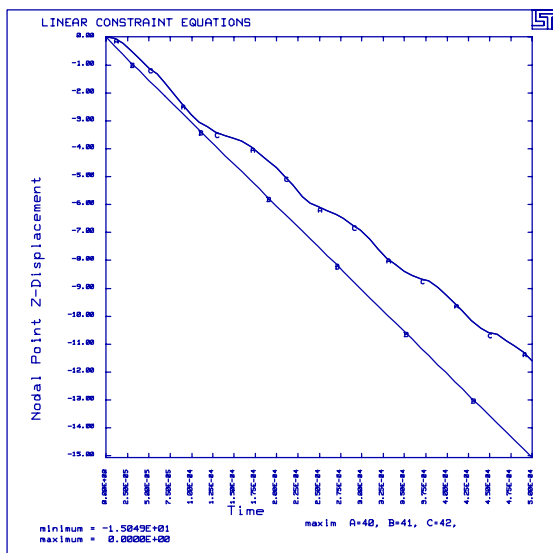
Linearly Constrained Plate

Results:

taurus g=d3plot
19
time 5e-4 rx -20 ndplt



phs3
nodout
z-disp



***CONSTRAINED_LINEAR**
Linearly Constrained Plate

***CONSTRAINED_SHELL_TO_SOLID** Impulsively Loaded Cap with Shells and Solids

LS-DYNA Manual Section: *CONSTRAINED_SHELL_TO_SOLID

Additional Sections:

*LOAD_SEGMENT

Example: Impulsively Loaded Cap with Shells and Solids

Filename: constrained.shell_solid.dome.k

Description:

A dome has an impulsive pressure load. The dome contains shell and brick element joined with shell-brick interfaces.

Model:

Only 1/4 of the dome is modeled due to symmetry. The dome shells are Hughes-Liu shell elements with three integration point through the thickness. Four shell elements have a pressure load of 5,308 psi over 0.0017246 square inches. The termination time is 0.0004 seconds.

Input:

The model contains one shell-brick group that has 7 shell nodes tied to 5 brick node (*CONSTRAINED_SHELL_TO_SOLID). The model contains four pressure surfaces (*LOAD_SEGMENT). Five nodes are written to the time history ASCII database file nodout (*DATABASE_HISTORY_NODE, *DATABASE_NODOUT).

Results:

The plots show the response of the dome.

Reference:

T. Littlewood

*CONSTRAINED_SHELL_TO_SOLID

Impulsively Loaded Cap with Shells and Solids

```

$
*SET_NODE_LIST
$   sid      da1      da2      da3      da4
$     5
$   nid1     nid2     nid3     nid4     nid5     nid6     nid7     nid8
$   120     162     204     246     288
$
$
$
*CONSTRAINED_SHELL_TO_SOLID
$   nid      nsid
$   331       6
$
*SET_NODE_LIST
$   sid      da1      da2      da3      da4
$     6
$   nid1     nid2     nid3     nid4     nid5     nid6     nid7     nid8
$   121     163     205     247     289
$
$
$
*CONSTRAINED_SHELL_TO_SOLID
$   nid      nsid
$   332       7
$
*SET_NODE_LIST
$   sid      da1      da2      da3      da4
$     7
$   nid1     nid2     nid3     nid4     nid5     nid6     nid7     nid8
$   122     164     206     248     290
$
$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Loads
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Load 4 segments with pressure at 5,308 psi for 2.0E-04 seconds
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*LOAD_SEGMENT
$   lcid      sf      at      n1      n2      n3      n4
$     1 1.000E+00 0.000E+00      1      2      4      3
$     1 1.000E+00 0.000E+00      2      5      7      4
$     1 1.000E+00 0.000E+00      3      4      8      6
$     1 1.000E+00 0.000E+00      4      7      9      8
$
*DEFINE_CURVE
$   lcid      sidr      scla      sclo      offa      offo
$     1
$
$
$           a           o
$     0.000E+00      5.308E+04
$     2.000E-04      5.308E+04
$     2.010E-04      0.000E+00
$     1.000E+00      0.000E+00
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8

```


***CONSTRAINED_SHELL_TO_SOLID**
Impulsively Loaded Cap with Shells and Solids

```

.
202      2      280      281      44      43      322      323      21      20
203      2      281      282      45      44      323      324      22      21
204      2      282      283      46      45      324      325      23      22
$
$$$$$ Elements - Shells
$
*ELEMENT_SHELL
$  eid      pid      n1      n2      n3      n4
   1         3      326      333      334      327
   2         3      327      334      335      328
   3         3      328      335      336      329
.
... in total, 60 shells defined
.
58      3      392      399      400      393
59      3      393      400      401      394
60      3      394      401      402      395
$
*END

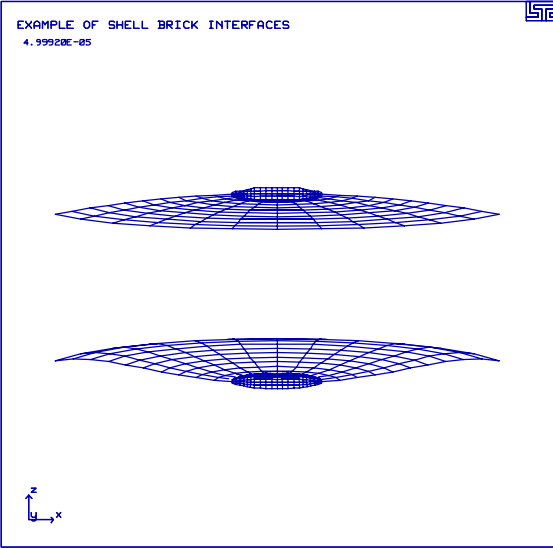
```

*CONSTRAINED_SHELL_TO_SOLID

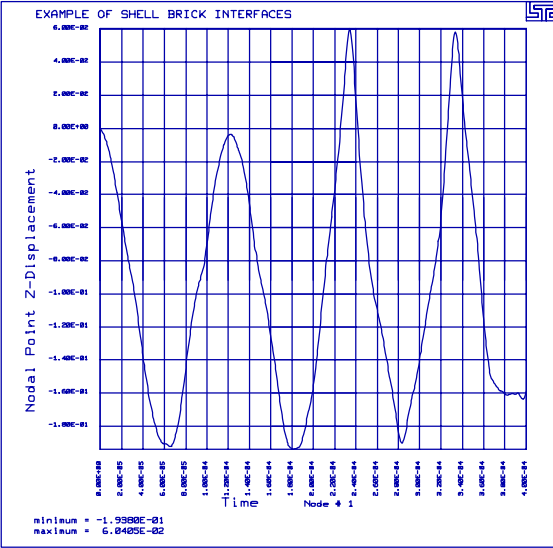
Impulsively Loaded Cap with Shells and Solids

Results:

```
taurus g=d3plot  
19  
rayz rx -90 center ytran .3 v ytran -.6 s 6 over v
```



```
phs3  
nodout  
grid z-disp  
1
```



***CONSTRAINED_SHELL_TO_SOLID**
Impulsively Loaded Cap with Shells and Solids

LS-DYNA Manual Section: *CONSTRAINED_SPOTWELD

Additional Sections:

*BOUNDARY_PRESCRIBED_MOTION_SET
*DATABASE_CROSS_SECTION_PLANE
*DATABASE_CROSS_SECTION_SET

Example: Spot Weld Secures Two Plates

Filename: constrained.spotweld.plates.k

Description:

Two overlapping plates are connected using three spotwelds. The plates are pulled apart until the spot welds reach the defined failure condition.

Model:

The two plates measure $80 \times 40 \times 1 \text{ mm}^3$ and are defined with S/R Hughes-Liu shell elements to control hourglassing. The location of the spotwelds connecting the two plates is in the center of the overlapping section. One end of the plate has fixed constraints and the other end of the other plate has linearly increasing displacement.

Input:

The nodal point cards contain the boundary conditions at one end of the plate (*NODES). *BOUNDARY_PRESCRIBED_MOTION_SET defines the nodal motion of the end of the other plate. Massless beams simulate the connection between the plates at three locations (*CONSTRAINED_SPOTWELD). The definitions include failure as a function of the axial and shear force.

The ASCII file swforc contains the axial and shear forces on the spotweld (*DATABASE_SWFORC). A cross section is defined through each of the plates using two different techniques (*DATABASE_CROSS_SECTION_PLANE, *DATABASE_CROSS_SECTION_SET). Forces and moments through the cross sections are stored in the ASCII file secforc (*DATABASE_SECFORC).

***CONSTRAINED_SPOTWELD**
Spot Weld Secures Two Plates

```

    201
$
*SET_NODE_LIST
$   sid
    201
$   nid1      nid2      nid3      nid4      nid5      nid6      nid7      nid8
    213        123
$
*DATABASE_NODOUT
$   dt
    0.010
$
*DATABASE_HISTORY_NODE
$   id1      id2      id3      id4      id5      id6      id7      id8
    123      233
$
*DATABASE_SECFORC
$   dt
    0.010
$
*DATABASE_SWFORC
$   dt
    0.010
$
$
$
$$$$$ Constrain the Plates Together
$
$$$$$ Three spotwelds across the plate, with failure defined.
$
*CONSTRAINED_SPOTWELD
$   n1      n2      sn      sf      n      m
    212      122      7.854   4.534   2.0    2.0
    213      123      7.854   4.534   2.0    2.0
    214      124      7.854   4.534   2.0    2.0
$
$
$$$$$ Boundary Motion Conditions
$
$$$$$ Prescribe the velocity of the nodes on one end of the plate.
$
*BOUNDARY_PRESCRIBED_MOTION_SET
$   nid      dof      vad      lcid      sf      vid
    1         1         0         1         1.0    0
$
*DEFINE_CURVE
$   lcid      sidr      scla      sclo      offa      offo
    1
$   abscissa      ordinate
           0.0000      0.0
           10.0000     0.3048
           20.0000     0.3048
$
*SET_NODE_LIST
$   sid
    1

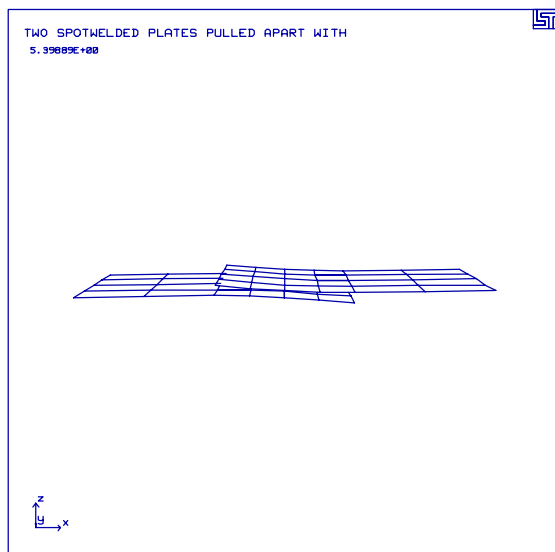
```

*CONSTRAINED_SPOTWELD

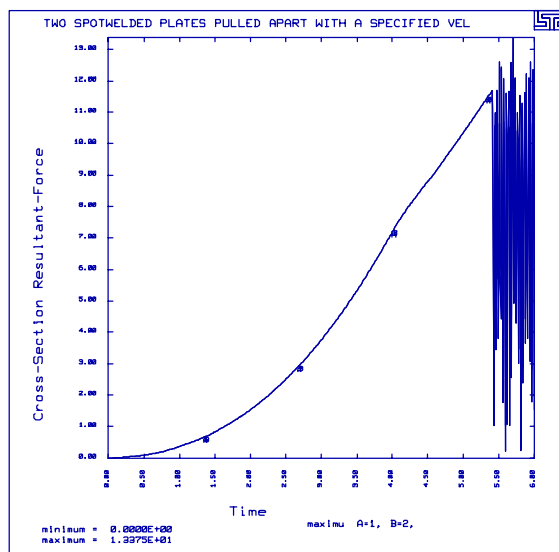
Spot Weld Secures Two Plates

Results:

taurus g=d3plot
19
rx -80 state 28 view



phs3
secforc
aset 0 6 r-forc



LS-DYNA Manual Section: *CONTACT

Additional Sections:

*INITIAL_VELOCITY

Example: Shell Rebounds from Plate Using Five Contact Types

Filename: contact.plates.k

Description:

A shell element drops and rebounds on an elastic plate.

Model:

The plate measures $40 \times 40 \times 1 \text{ mm}^3$ and contains 16 shell elements. The dropped shell element has a side length of 10 mm, a thickness of 2 mm and drop height of 10 mm. All shell elements are elastic with Belytschko-Tsay formulation. The dropped shell element has an initial velocity of 100,000 mm/second vertically towards the plate. The calculations terminate at 0.0002 seconds.

Input:

All four nodes of the dropped shell element have an initial velocity specified by *INITIAL_VELOCITY. Contact types 3, 5 and 10 use the dropped shell element as slave side and the four shell elements in the center of the plate as master side. The example file has type 3 contact activated, while the other contact types are commented out. To change contact types, simply comment out type 3 and un-comment the desired contact.

Type 3 contact is a two way surface to surface algorithm. The segments on the slave side are checked for penetration of the master segment then the opposite search takes place.

Type 4 is a single surface algorithm. The nodes of all segments are checked for penetration of all segments.

Type 5 is a node to surface one way algorithm. The program checks that no slave node penetrates any master segment.

Type 10 converts surface to surface definition into a node to surface definition.

Type 13 is a more robust version of the single surface algorithm.

Reference:

Schweizerhof, K. and Weimer, K.

Shell Rebounds from Plate Using Five Contact Types

```
$      dt
      0.01e-04
$
*DATABASE_HISTORY_NODE
$      id1      id2      id3      id4      id5      id6      id7      id8
       12       13       101
$
*DATABASE_MATSUM
$      dt
      0.10e-05
$
*DATABASE_RCFORC
$      dt
      0.01e-04
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Contacts
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
$$$$$$$$ Type 3, surface to surface
$
*CONTACT_SURFACE_TO_SURFACE
$      ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
        1         2         dc         vc         vdc        penchk        bt         dt
$
        sfs       sfm       sst       mst       sfst       sfmt       fsf       vsf
$
*SET_SEGMENT
$      sid
        1
$      n1      n2      n3      n4
       101     103     104     102
$
*SET_SEGMENT
$      sid
        2
$      n1      n2      n3      n4
         7         8         13        12
         8         9         14        13
        12        13        18        17
        13        14        19        18
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
$$$$$$$$ Type 4, single surface
$
      to make active, remove the $$ from the lines below
$
$$*CONTACT_SINGLE_SURFACE
$      ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
$$      1         0
$      fs       fd       dc       vc       vdc       penchk       bt       dt
$$
$      sfs       sfm       sst       mst       sfst       sfmt       fsf       vsf
$$
$
$$*SET_SEGMENT
$      sid
```

*CONTACT

Shell Rebounds from Plate Using Five Contact Types

```
$$      1
$      n1      n2      n3      n4
$$     101     103     104     102
$$      7      8      13     12
$$      8      9      14     13
$$     12     13     18     17
$$     13     14     19     18
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
$$$$$$$$ Type 5, node to surface
$          to make active, remove the $$ from the lines below
$
$$*CONTACT_NODES_TO_SURFACE
$  ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
$$      1      2      4      1      1
$      fs      fd      dc      vc      vdc      penchk      bt      dt
$$
$      sfs      sfm      sst      mst      sfst      sfmt      fsf      vsf
$$
$
$$*SET_NODE_LIST
$  sid
$$      1
$  nid1      nid2      nid3      nid4      nid5      nid6      nid7      nid8
$$      101      103      104      102
$
$$*SET_SEGMENT
$  sid
$$      2
$  n1      n2      n3      n4
$$      7      8      13     12
$$      8      9      14     13
$$     12     13     18     17
$$     13     14     19     18
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
$$$$$$$$ Type 10, surface to surface
$          to make active, remove the $$ from the lines below
$
$$*CONTACT_ONE_WAY_SURFACE_TO_SURFACE
$  ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
$$      1      2      1      1
$      fs      fd      dc      vc      vdc      penchk      bt      dt
$$
$      sfs      sfm      sst      mst      sfst      sfmt      fsf      vsf
$$
$
$$*SET_SEGMENT
$  sid
$$      1
$  n1      n2      n3      n4
$$     101     103     104     102
$
$$*SET_SEGMENT
$  sid      da1      da2      da3      da4
$$      2
$  n1      n2      n3      n4
$$      7      8      13     12
$$      8      9      14     13
$$     12     13     18     17
$$     13     14     19     18
```


***CONTACT**

Shell Rebounds from Plate Using Five Contact Types

16	1	19	20	25	24
101	2	101	102	104	103

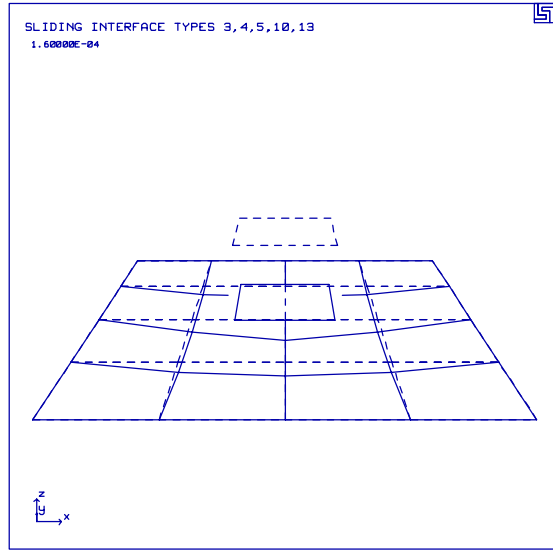
\$
*END

*CONTACT

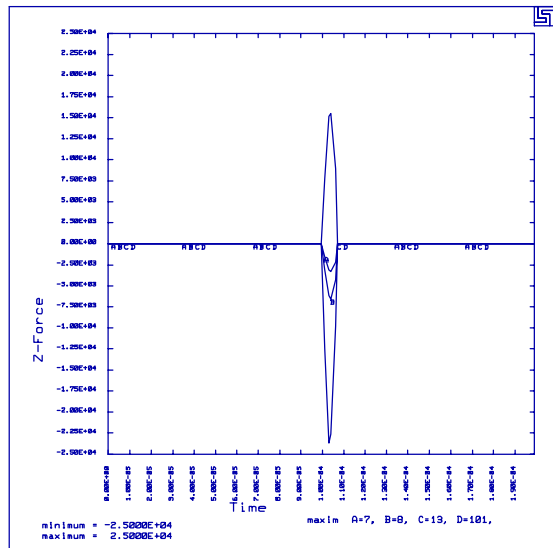
Shell Rebounds from Plate Using Five Contact Types

Results:

taurus g=d3plot
19
udg 1 time 1.6e-4 rx -70 view



phs3
ncforc
oset -2.5e4 2.5e4 z-forc 7 8 13 101



***CONTACT_ERODING_SURFACE_TO_SURFACE** Projectile Penetrates Plate

LS-DYNA Manual Section: *CONTACT_ERODING_SURFACE_TO_SURFACE

Additional Sections:

*INITIAL_VELOCITY_GENERATION

Example: Projectile Penetrates Plate

Filename: contact.projectile.k

Description:

A projectile strikes a plate at a critical angle.

Model:

The hemispherical projectile has a length of 7.67 cm and a diameter of 0.767 cm. The plate measures 23.01 cm × 23 cm × 0.64 cm. The projectile and the plate are elastic perfectly plastic with failure strain. The initial velocity of the projectile is 0.129 cm/μsec at an angle of 75 degrees. The calculation terminates at 110.0 μsec.

Input:

The initial velocity (magnitude and direction) of the projectile is set using *INITIAL_VELOCITY_GENERATION. Eroding contact between the projectile surface and plate surface is defined so that the contact erodes as the element erodes (*CONTACT_ERODING_SURFACE_TO_SURFACE). This allows the contact to work correctly as layers of the parts erode during penetration.

Results:

The projectile fractures into a tip and trailing portion. The trailing portion punches a hole through the plate while the tip deflects off the plate.

***CONTACT_ERODING_SURFACE_TO_SURFACE**
Projectile Penetrates Plate

```
*DATABASE_RCFORC
$   dt
    0.10
$
*DATABASE_SLEOUT
$   dt
    0.10
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Contacts
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$   ssid      msid      sstyp     mstyp     sboxid     mboxid     spr         mpr
    1         2         3         3
$
$   fs        fd        dc        vc        vdc        penchk     bt         dt
$
$   sfs       sfm       sst       mst       sfst       sfmt       fsf        vsf
$
$   isym      erosop     iadj
    1         1
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Initial Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Assign an initial velocity to the projectile (part 1) angled down
$$$$$ towards the plate.
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*INITIAL_VELOCITY_GENERATION
$   sid      styp     omega      vx         vy         vz
    1         1         1.246E-01 0.000E+00 -3.339E-02
$
$   xc       yc       zc       nx       ny       nz        phase
$
$
*SET_PART
    1
    1
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*PART
$   pid      sid      mid      eosid     hgid     adpopt
Projectile
```

***CONTACT_ERODING_SURFACE_TO_SURFACE**

Projectile Penetrates Plate

```

          1          1          1
Plate    2          1          2

```

```

$$$ Materials

```

```

$$$ failure strain for erosion of the projectile and plate elements are
$$$ set as: fs = 0.8

```

```

*MAT_PLASTIC_KINEMATIC

```

```

$ mid ro e pr sigy etan beta
$ 1 1.862E+01 1.170E+00 0.22 1.790E-02 1.0
$ src srp fs
$ 0.8

```

```

*MAT_PLASTIC_KINEMATIC

```

```

$ mid ro e pr sigy etan beta
$ 2 7.896E+00 2.100E+00 0.284 1.000E-02 1.0
$ src srp fs
$ 0.8

```

```

$$$$ Sections

```

```

*SECTION_SOLID

```

```

$ sid elform
$ 1 0

```

```

$$$$ Define Nodes and Elements

```

```

*NODE

```

```

$ node x y z tc rc
$ 1 9.241751E+00 -1.534000E-05 5.137928E-02 2 6
$ 2 9.193813E+00 0.000000E+00 1.344095E-01 2 6
$ 3 9.145876E+00 0.000000E+00 2.174397E-01 2 6
$ ... in total, 7668 nodes defined
$ 7666 1.918446E+01 4.800000E+00 0.000000E+00 7 7
$ 7667 2.071067E+01 4.800000E+00 0.000000E+00 7 7
$ 7668 2.300000E+01 4.800000E+00 0.000000E+00 7 7

```

```

$$$$ Elements

```

```

*ELEMENT_SOLID

```

```

$ eid pid n1 n2 n3 n4 n5 n6 n7 n8
$ 1 1 1 2 5 4 10 11 14 13
$ 2 1 2 3 6 5 11 12 15 14
$ 3 1 4 5 8 7 13 14 17 16
$ ... in total, 5664 solids defined
$ 5662 2 7617 7618 7626 7625 7657 7658 7666 7665
$ 5663 2 7618 7619 7627 7626 7658 7659 7667 7666

```

***CONTACT_ERODING_SURFACE_TO_SURFACE**
Projectile Penetrates Plate

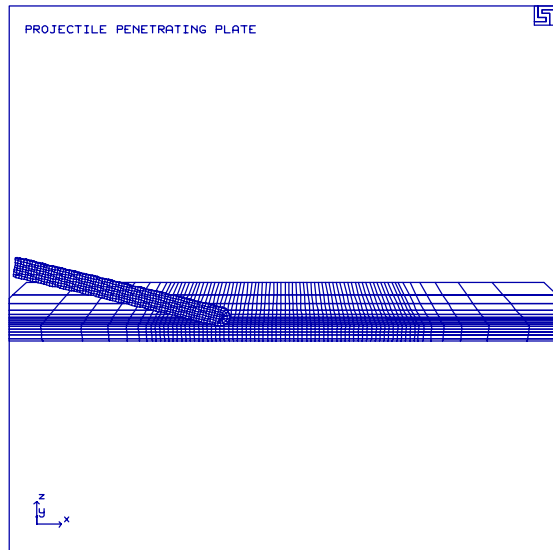
5664 2 7619 7620 7628 7627 7659 7660 7668 7667
\$
*END

*CONTACT_ERODING_SURFACE_TO_SURFACE

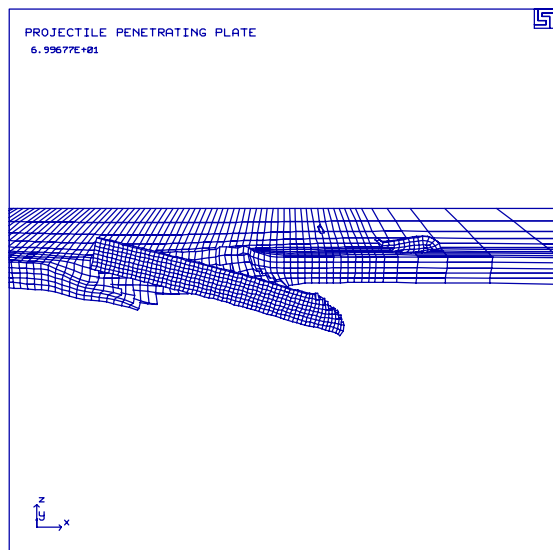
Projectile Penetrates Plate

Results:

taurus g=d3plot
19
rx -70 dist 27 view



state 8
m 1 center
dam view



*CONTACT_NODES_TO_SURFACE

Rigid Sphere Impacts a Plate at High Speed

LS-DYNA Manual Section: *CONTACT_NODES_TO_SURFACE

Additional Sections:

*CONSTRAINED_TIED_NODES_FAILURE

Example: Rigid Sphere Impacts a Plate at High Speed

Filename: contact.n2s-sphere.k

Description:

A sphere impacts a plate at high speed causing failure of the plate. This model can be used to show how different contacts can behave differently in a rather simple model. Instructions of this are explained in the header of the input deck.

Model:

A rigid sphere is made out of solid elements and given an initial velocity of 89 mm/ms towards a plate using the *DEFINE_BOX keyword. The plate is constructed out of shell elements. The shells of the plates do NOT have their nodes merged at common locations. Instead, tied nodes with failure constraints are used to connect the common nodes. This allows the plate to rupture and rip along seam lines instead of having elements fail (and being deleted) by using the more common failure criteria within the material definition.

Results:

The plate is definitely not made out of a bullet proof material.

*CONTACT_NODES_TO_SURFACE

Rigid Sphere Impacts a Plate at High Speed

```

*DATABASE_BINARY_D3THDT
$    dt      lcdt
    999999
$
*DATABASE_GLSTAT
$    dt
    0.005
$
*DATABASE_MATSUM
$    dt
    0.005
$
*DATABASE_NODOUT
$    dt
    0.005
$
*DATABASE_HISTORY_NODE
$    id1      id2      id3      id4      id5      id6      id7      id8
    2633      362      489
$
*DATABASE_RBDOUT
$    dt
    0.005
$
*DATABASE_RCFORC
$    dt
    0.005
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Initial Velocity
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
*INITIAL_VELOCITY
$
$    nsid      nsidex      boxid
                              5
$
$    vx      vy      vz      wx      wy      wz
    0.0      0.0      -89.0
$
*DEFINE_BOX
$
$    boxid      xmm      xmx      ymn      ymx      zmn      zmx
    5      -39.0      39.0      -39.0      39.0      -25.41      51.0
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Contacts - sliding interface definitions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$. . . > . . . 1 . . . > . . . 2 . . . > . . . 3 . . . > . . . 4 . . . > . . . 5 . . . > . . . 6 . . . > . . . 7 . . . > . . . 8
$
*CONTACT_NODES_TO_SURFACE
$
$    ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
    2      3      3      3
$
$    fs      fd      dc      vc      vdc      penchk      bt      dt
$
$

```

***CONTACT_NODES_TO_SURFACE**
Rigid Sphere Impacts a Plate at High Speed

```

$ sfs sfm sst mst sfst sfmt fsf vsf
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*PART
$
$ pid sid mid eosid hgid grav adpopt
plate 2 1 1
sphere 3 2 2
$
$
$$$$ Materials
$
*MAT_PIECEWISE_LINEAR_PLASTICITY
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$ mid ro e pr sigy etan eppf tdel
1 0.783E-05 200.0 0.3 0.207 0.750
$ Cowper/Symonds Strain Rate Parameters
$ c p lcss lcsr
40 5
$ Plastic stress/strain curves
0.000 0.080 0.160 0.400 1.000
0.207 0.250 0.275 0.290 0.300
$
$
*MAT_RIGID
$
$ mid ro e pr n couple m alias
2 0.783E-05 200.0 0.3
$
$ cmo con1 con2
$
$ lco/a1 a2 a3 v1 v2 v3
$
$
$$$$ Sections
$
*SECTION_SHELL
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$ sid elform shrf nip propt qr/irid icomp
1 2 3.0
$ t1 t2 t3 t4 nloc
2.50 2.50 2.50 2.50
$
*SECTION_SOLID
$
$ sid elform
2
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$

```


*CONTACT_NODES_TO_SURFACE

Rigid Sphere Impacts a Plate at High Speed

```

$
$$$$ Define Tied Nodes with Failure Constraints
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>....1.>....2.>....3.>....4.>....5.>....6.>....7.>....8
$
$$$$ Tie all the adjacent corners of the shells together. Essentially, do
$$$$ a merge by way of tied nodes with failure.
$
*CONSTRAINED_TIED_NODES_FAILURE
$   nsid      eppf
     101      0.0850
$
*SET_NODE_LIST
$   sid
     101
     775      778      896      897
$
.
... in total, 841 CONSTRAINED_TIED_NODES_FAILURE/SET_NODE_LIST pairs defined
.
$
*CONSTRAINED_TIED_NODES_FAILURE
$   nsid      eppf
     941      0.0850
*SET_NODE_LIST
$   sid
     941
     4247      4250      4368      4369
*END

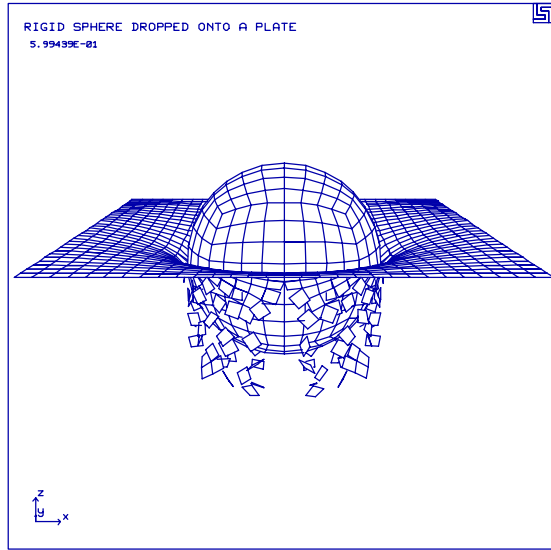
```

*CONTACT_NODES_TO_SURFACE

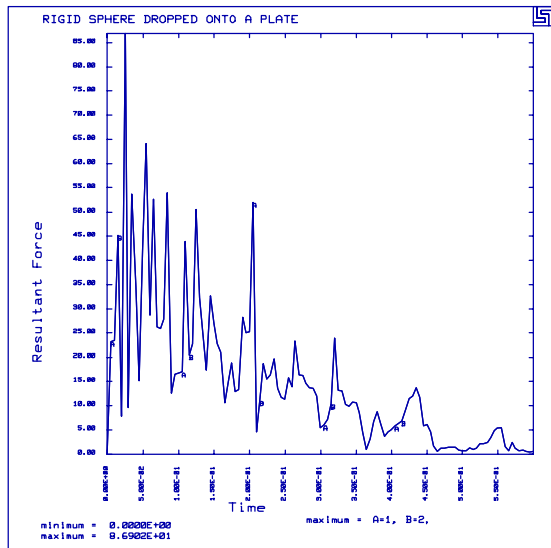
Rigid Sphere Impacts a Plate at High Speed

Results:

taurus g=d3plot
state 7 center
rx -75 view



phs3
rforc
result



***CONTACT_NODES_TO_SURFACE**
Rigid Sphere Impacts a Plate at High Speed

LS-DYNA Manual Section: *CONTACT_SINGLE_EDGE

Additional Sections:

*CONTACT_FORCE_TRANSDUCER_PENALTY

Example: Corrugated Sheet Contacts Edges

Filename: contact.edge.k

Description:

A corrugated plate strikes a flat plate from opposite directions.

Input:

The model consists of 135 elastic plastic Belytschko-Tsay shell elements. The interaction of the two structures is to edge contact (*CONTACT_SINGLE_EDGE). A contact force transducer is defined to monitor the forces of the contact in the ascii file rforc. The nodes on the upper corrugated plate have an initial velocity of 10 meters/second.

Results:

A contour plot of the effective-stress and a plot of the forces from the ascii file rforc illustrate that the plates are in contact.

Reference:

Stillman, D. W.

*CONTACT_SINGLE_EDGE

Corrugated Sheet Contacts Edges

List of LS-DYNA input deck:

```
*KEYWORD
*TITLE
Edge to Edge Contact with Force Transducer
$
$  LSTC Example
$
$  Last Modified: September 9, 1997
$
$  Units: kg, m, s, N, Pa, Joule
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$$$  Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1.>...2.>...3.>...4.>...5.>...6.>...7.>...8
$
*CONTROL_TERMINATION
$  endtim  endcyc  dtmin  endneg  endmas
$    0.050
$
*CONTROL_HOURLASS
$  ihq      qh
$    4
$
*DATABASE_BINARY_D3PLOT
$  dt      lcdt
$    0.001
$
*DATABASE_BINARY_D3THDT
$  dt      lcdt
$    9.990E+02
$
*DATABASE_GLSTAT
$  dt
$    0.001
$
*DATABASE_MATSUM
$  dt
$    0.001
$
*DATABASE_RCFORC
$  dt
$    0.001
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$$$  Define Contacts
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1.>...2.>...3.>...4.>...5.>...6.>...7.>...8
$
$$$$$$$$$$$  Type 22, single edge contact
$
*CONTACT_SINGLE_EDGE
$  ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
$    1        1        0          0
$  fs        fd        dc         vc         vdc         penchk      bt       dt
```

***CONTACT_SINGLE_EDGE**
Corrugated Sheet Contacts Edges

\$	sfs	sfm	sst	mst	sfst	sfmt	fsf	vsf
\$								
*SET_SEGMENT								
\$	sid							
	1							
\$	n1	n2	n3	n4				
	1	2	0	0				
	2	3	0	0				
	3	13	0	0				
	13	14	0	0				
	14	21	0	0				
	21	22	0	0				
	22	29	0	0				
	29	30	0	0				
	30	37	0	0				
	37	38	0	0				
	38	45	0	0				
	45	46	0	0				
	46	53	0	0				
	53	54	0	0				
	54	61	0	0				
	61	62	0	0				
	69	70	0	0				
	70	71	0	0				
	71	72	0	0				
	72	73	0	0				
	73	74	0	0				
	74	75	0	0				
	75	76	0	0				
	76	77	0	0				
	77	78	0	0				
	78	79	0	0				
	79	80	0	0				
	80	81	0	0				
	81	82	0	0				
	111	112	0	0				
	112	113	0	0				
	113	114	0	0				
	114	115	0	0				
	115	116	0	0				
	116	117	0	0				
	117	118	0	0				
	118	119	0	0				
	119	120	0	0				
	120	121	0	0				
	121	122	0	0				
	122	123	0	0				
	123	124	0	0				
	125	126	0	0				
	126	127	0	0				
	127	137	0	0				
	137	138	0	0				
	138	145	0	0				
	145	146	0	0				
	146	153	0	0				
	153	154	0	0				
	154	161	0	0				
	161	162	0	0				
	162	169	0	0				
	169	170	0	0				
	170	177	0	0				
	177	178	0	0				

***CONTACT_SINGLE_EDGE**
Corrugated Sheet Contacts Edges

178 185 0 0
185 186 0 0

\$
\$
\$\$\$\$ Force transducer defined to calculate contact forces on part 1.
\$
*CONTACT_FORCE_TRANSDUCER_PENALTY
\$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
\$ ssid msid sstyp mstyp
 5 2

\$
*SET_PART_LIST
\$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
 5
 1

\$
\$\$\$\$
\$
\$\$\$\$ Initial Conditions
\$
\$\$\$\$
\$
\$\$\$\$ Nodes of the part 1 (node set id = 2) are given an initial velocity
\$\$\$\$ in the y-direction of 10 m/s.

\$
*INITIAL_VELOCITY
\$ nsid nsidex boxid
 2
\$ vx vy vz vxr vyr vzy
 0.0 10.0 0.0 0.0 0.0 0.0

\$
*SET_NODE_LIST
\$ sid
 2
\$ nid1 nid2 nid3 nid4 nid5 nid6 nid7 nid8
 1 2 3 4 5 6 7 8
 9 10 11 12 13 14 15 16
 17 18 19 20 21 22 23 24
 25 26 27 28 29 30 31 32
 33 34 35 36 37 38 39 40
 41 42 43 44 45 46 47 48
 49 50 51 52 53 54 55 56
 57 58 59 60 61 62 63 64
 65 66 67 68

\$
\$\$\$\$
\$
\$\$\$\$ Define Parts and Materials
\$
\$\$\$\$
\$
\$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8

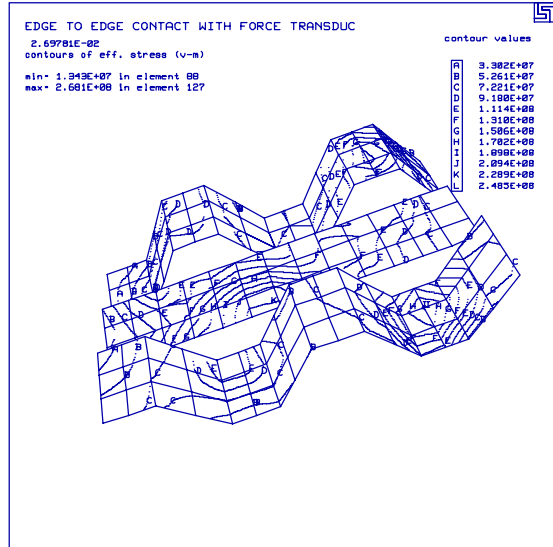
\$
*PART
\$ pid sid mid eosid hgid adpopt
plate-1 1 1 1
plate-2 2 1 1
plate-3

*CONTACT_SINGLE_EDGE

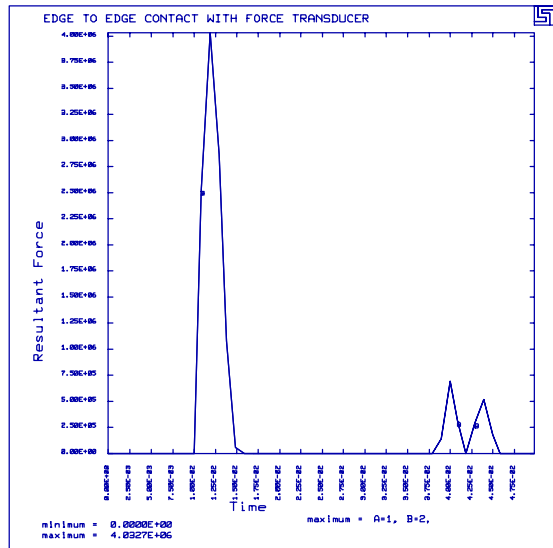
Corrugated Sheet Contacts Edges

Results:

taurus g=d3plot
 19
 rx -40 rz 20 s 28 mono numc 12 contour 9



phs3
 rforc
 resultant



*CONTACT_TIED_NODES_TO_SURFACE

Discrete Nodes Tied to a Surface

LS-DYNA Manual Section: *CONTACT_TIED_NODES_TO_SURFACE

Example: Discrete Nodes Tied to a Surface

Filename: contact.tied_nodes.box.k

Description:

A shell element drops onto and then rebounds from, a hollow box that is tied to an elastic plate.

Model:

The plate measures $40 \times 40 \times 1 \text{ mm}^3$ and contains 16 Belytschko-Tsay shell elements. The dropped shell element has a side length of 10 mm, a thickness of 2 mm and a drop height of 10 mm. The box contains 12 Belytschko-Tsay shell elements. All shell element materials are elastic. The initial velocity of the shell elements is 100,000 mm/second. The calculation terminates at 0.002 seconds.

Input:

The nodes of the dropped shell are given an initial velocity (*INITIAL_VELOCITY). The nodes on the bottom of the box, those facing the plate, are tied to the plate (*CONTACT_TIED_NODES_TO_SURFACE). Automatic single surface contact is used to define the contact between the dropped shell and the box.

Reference:

Schweizerhof, K. and Weimer, K.

***CONTACT_TIED_NODES_TO_SURFACE**

Discrete Nodes Tied to a Surface

List of LS-DYNA input deck:

```
*KEYWORD
*TITLE
Sliding Interface Type 6
$
$   LSTC Example
$
$   Last Modified: September 5, 1997
$
$   A box is tied to a bottom plate with tied nodes to surface contact.
$   This box is impacted by a shell element, which has an initial velocity.
$
$   Units: mm, s
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$$$ Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
*CONTROL_TERMINATION
$   endtim   endcyc   dtmin   endneg   endmas
$   0.200E-03
$
*CONTROL_HOURLASS
$   ihq       qh
$           4
$
$
*DATABASE_BINARY_D3PLOT
$   dt       lcdt
$   0.010E-03
$
*DATABASE_BINARY_D3THDT
$   dt       lcdt
$   .0005E-03
$
$
*DATABASE_NODOUT
$   dt
$   .0010E-03
$
*DATABASE_HISTORY_NODE
$   id1      id2      id3      id4      id5      id6      id7      id8
$   101      13       213
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$ Define Contacts
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1.>...2.>...3.>...4.>...5.>...6.>...7.>...8
$
*CONTACT_AUTOMATIC_SINGLE_SURFACE
$   ssid      msid      sstyp    mstyp    sboxid    mboxid    spr       mpr
$           0
$   fs        fd         dc        vc        vdc       penchk    bt        dt
$   sfs       sfm       sst       mst       sfst      sfmt      fsf       vsf
```


*CONTACT_TIED_NODES_TO_SURFACE

Discrete Nodes Tied to a Surface

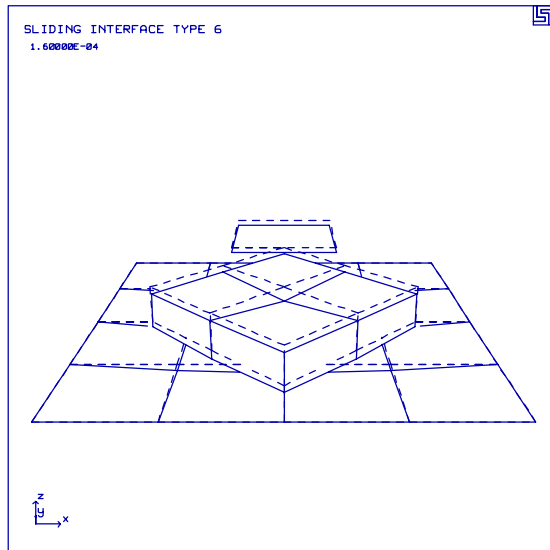
```
$
*SECTION_SHELL
$   sid   elform   shrf   nip   propt   qr/irid   icomp
$     1     1       0.83333   2     propt   qr/irid   icomp
$   t1     t2     t3     t4     nloc
$     1.0     1.0     1.0     1.0
$
*SECTION_SHELL
$   sid   elform   shrf   nip   propt   qr/irid   icomp
$     2     1       0.83333   2     propt   qr/irid   icomp
$   t1     t2     t3     t4     nloc
$     2.0     2.0     2.0     2.0
$
$$$$$ Define Nodes and Elements
$
$$$$$ Outer edge nodes of the bottom plate (part 1)
$$$$$ are fixed in translation (tc = 7)
$
*NODE
$   node      x      y      z      tc      rc
$     1  0.000000E+00  0.000000E+00  0.000000E+00  7  0
$     2  1.000000E+01  0.000000E+00  0.000000E+00  7  0
$     3  2.000000E+01  0.000000E+00  0.000000E+00  7  0
$     .
$     ... in total, 48 nodes defined
$     .
$    217  5.867900E+00  2.000000E+01  4.000000E+00  0  0
$    218  1.292890E+01  2.707110E+01  4.000000E+00  0  0
$    219  2.000000E+01  3.414210E+01  4.000000E+00  0  0
$
$$$$$ SHELL ELEMENTS
$
*ELEMENT_SHELL
$   eid   pid   n1   n2   n3   n4
$     1     1     1     2     7     6
$     2     1     2     3     8     7
$     3     1     3     4     9     8
$     .
$     ... in total, 29 shells defined
$     .
$    210     3    212    213    216    215
$    211     3    214    215    218    217
$    212     3    215    216    219    218
$
*END
```

*CONTACT_TIED_NODES_TO_SURFACE

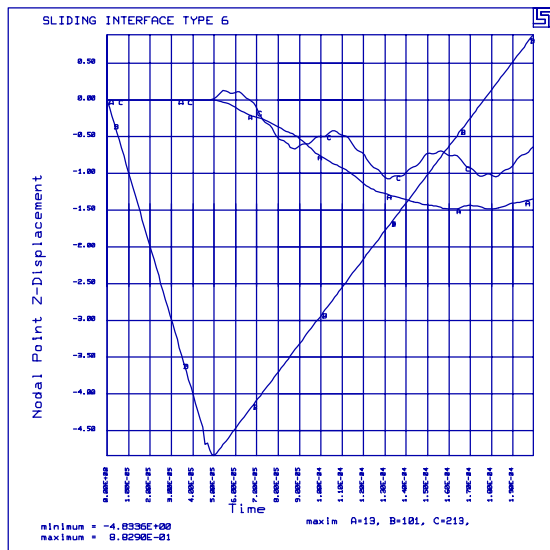
Discrete Nodes Tied to a Surface

Results:

taurus g=d3plot
19
udg 1 time 1.6e-4 rx -70 view



phs3
nodout
grid z-disp



***CONTACT_TIED_NODES_TO_SURFACE**

Discrete Nodes Tied to a Surface

LS-DYNA Manual Section: *CONTACT_ENTITY

Additional Sections:

*BOUNDARY_PRESCRIBED_MOTION_RIGID

Example: Rigid Sphere Impacts Plate

Filename: contact_entity.sphere.k

Description:

A rigid sphere drops onto an elastic plate. The sphere contains shell elements automatically generated with a “Geometric Contact Entity” spherical surface.

Model:

The plate of elastic material measures $40 \times 40 \times 2 \text{ mm}^3$ and contains 64 Belytschko-Tsay shell elements. The sphere has a radius of 6.0 mm and the distance from the center of the cube to the plate is 8.5 mm. The inertia properties of the sphere are defined by the properties of the rigid brick element. A geometric contact entity defines the spherical contact surface. The sphere moves toward the plate with a uniform motion. The termination time is 0.0005 seconds.

Input:

The Geometric Contact Entity defines the outer master surface on the rigid sphere (*CONTACT_ENTITY). The nodes on the plate are slave nodes (*SET_NODE_LIST), and are in the “Geometric Entity”. A load curve definition defines the movement of the sphere (*BOUNDARY_PRESCRIBED_MOTION_RIGID, *DEFINE_CURVE). The displacement condition for rigid bodies is input by part number, not by listing the nodes included in the definition.

Reference:

Schweizerhof, K. and Weimer, K.

***CONTACT_ENTITY**
Rigid Sphere Impacts Plate

```

$$$$ Contact Entity
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1....>...2....>...3....>...4....>...5....>...6....>...7....>...8
$
*CONTACT_ENTITY
$   pid   geotyp   sid   styp   sf   df   cf   intord
$     2     2     1     0    1.0   df   cf   intord
$
$   bt     dt     so
$
$
$   xc     yc     zc     ax     ay     az
$  0.00   0.00   .00    1.00   0.00   0.00
$
$   bx     by     bz
$  0.00   1.00   0.00
$
$   inout   g1     g2     g3     g4     g5     g6     g7
$     0    20.00  20.00   9.00   6.00
$
$
*SET_NODE_LIST
$   sid     da1     da2     da3     da4
$     1
$
$   nid1     nid2     nid3     nid4     nid5     nid6     nid7     nid8
$     1         2         3         4         5         6         7         8
$     9        10        11        12        13        14        15        16
$    17        18        19        20        21        22        23        24
$    25        26        27        28        29        30        31        32
$    33        34        35        36        37        38        39        40
$    41        42        43        44        45        46        47        48
$    49        50        51        52        53        54        55        56
$    57        58        59        60        61        62        63        64
$    65        66        67        68        69        70        71        72
$    73        74        75        76        77        78        79        80
$    81
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1....>...2....>...3....>...4....>...5....>...6....>...7....>...8
$
$$$ Part   1   shell: plate - elastic material
$
$$$ Part   2   solid: sphere - rigid material ==> contact entity
$
*PART
plate
$   pid   sid   mid   eosid   hgid   adpopt
$     1     1     1     0       0       0
$
*PART
sphere
$   pid   sid   mid   eosid   hgid   adpopt
$     2     2     2     0       0       0
$
$

```


***CONTACT_ENTITY**
Rigid Sphere Impacts Plate

```

      3    1.000000E+01    0.000000E+00    0.000000E+00    3    0
      .
      ... in total, 81 nodes defined
      .
      79    3.000000E+01    4.000000E+01    0.000000E+00    3    0
      80    3.500000E+01    4.000000E+01    0.000000E+00    3    0
      81    4.000000E+01    4.000000E+01    0.000000E+00    3    0
$
$$$$$ Elements
$
*ELEMENT_SHELL
$  eid      pid      n1      n2      n3      n4
   1         1         1         2         11        10
   2         1         2         3         12        11
   3         1         3         4         13        12
      .
      ... in total, 64 shells defined
      .
      62         1         69         70         79         78
      63         1         70         71         80         79
      64         1         71         72         81         80
$
*END

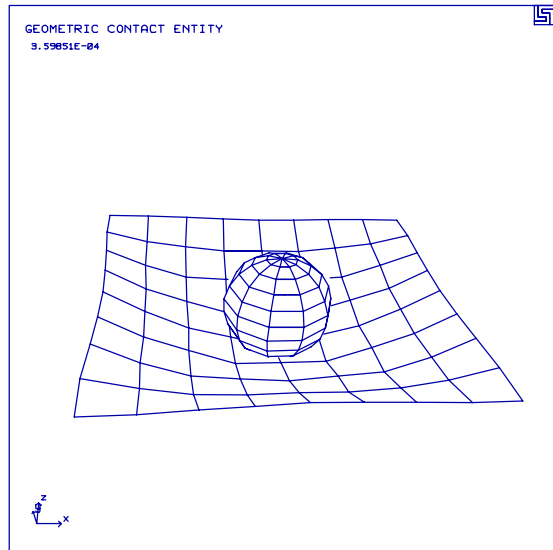
```

*CONTACT_ENTITY

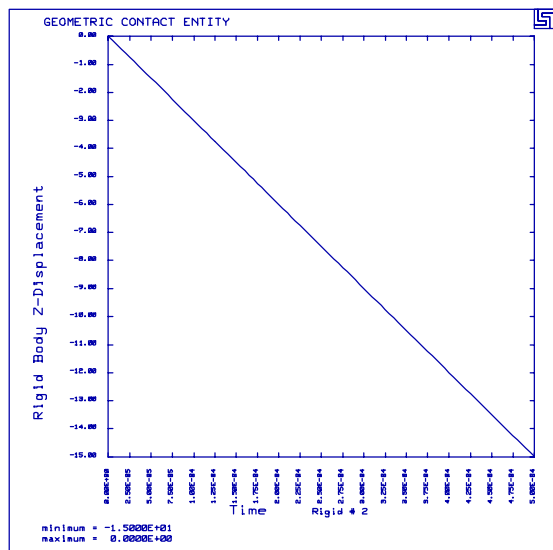
Rigid Sphere Impacts Plate

Results:

taurus g=d3plot
19
rx -60 ry 10 ytrans 5 s 19 view



phs3
rbdout
oset -15 0 z-disp



LS-DYNA Manual Section: *CONTROL_CONTACT

Additional Sections:

*LOAD_SEGMENT
*MAT_POWER_LAW_PLASTICITY
*RIGIDWALL_PLANAR

Example: Hemispherical Punch

Filename: control_contact.hemi-draw.k

Description:

This problem includes three tools a punch, a pressure pad, a die and a workpiece. A workpiece is deep drawn by the hemispherical punch while the pressure pad and die prevents wrinkling. The load on the pressure pad is ramped, then the punch displaces in the y direction.

Model:

The workpiece measures 80 mm in radius and 1 mm in thickness. The punch radius is 50.0 mm and the die torus radius is 6.35 mm. The workpiece contains 528 Belytschko Tsay shell elements with 5 integration points through the thickness. The tools are rigid members. Only 1/4 of the system is modeled because of symmetry.

Input:

The number of integration points is 5 for the workpiece. (*SECTION_SHELL) This model contains two options to consider shell thickness. The first option is the contact surfaces are projected to the true surface of shell (*CONTROL_CONTACT). The second option is membrane straining results in thickness changes (*CONTROL_CONTACT). The motion of the punch follows a sine function represented by load curve number 2 (Section 22).

Reference:

Honecker, A. and Mattiason, K.

*CONTROL_CONTACT

Hemispherical Punch

List of LS-DYNA input deck:

```

*KEYWORD
*TITLE
Hemispherical Deep Draw
$
$ LSTC Example
$
$ Last Modified: September 10, 1997
$
$ Units: kg, mm, ms, kN, GPa, kN-mm
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$. . . > . . . 1 . . . > . . . 2 . . . > . . . 3 . . . > . . . 4 . . . > . . . 5 . . . > . . . 6 . . . > . . . 7 . . . > . . . 8
$
*CONTROL_TERMINATION
$  endtim  endcyc  dtmin  endneg  endmas
      6.0
$
$$$$ shell thickness is considered during contact: shlthk = 1
$
*CONTROL_CONTACT
$  slsfac  rwpnal  islchk  shlthk  penopt  thkchg  orien
              1.0            1
$  usrstr  usrfac  nsbcs  interm  xpenen
$
$
*CONTROL_ENERGY
$  hgen  rwen  slnten  rylen
      2    2    2
$
$
*CONTROL_OUTPUT
$  npopt  neecho  nrefup  iaccop  opifs  ipnint  ikedit
      1    3      0      0      2      2      1000
$
$$$$ membrane straining causes thickness change: istupd = 1
$
*CONTROL_SHELL
$  wrpang  itrnst  irnxx  istupd  theory  bwc  miter
              1
$
$
*DATABASE_BINARY_D3PLOT
$  dt  lcdt
      0.20
$
$
*DATABASE_EXTENT_BINARY
$  neiph  neips  maxint  strflg  sigflg  epsflg  rltflg  engflg
              1
$  cmpflg  ieverp  beamip
              1
$
$
*DATABASE_BINARY_D3THDT
$  dt  lcdt
      12.00E+00
$
$
*DATABASE_GLSTAT

```

***CONTROL_CONTACT**
Hemispherical Punch

```
$      dt
      0.05
$
*DATABASE_MATSUM
$      dt
      0.05
$
*DATABASE_NODOUT
$      dt
      0.05
$
*DATABASE_HISTORY_NODE
$      id1         id2         id3         id4         id5         id6         id7         id8
      1333
$
*DATABASE_RCFORC
$      dt
      0.05
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Contacts
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
$$$$$$$$ contact between workpiece and punch
$
*CONTACT_SURFACE_TO_SURFACE
$      ssid       msid       sstyp       mstyp       sboxid       mboxid       spr         mpr
$            1         2         3         3         vdc          penchk       bt          dt
$      0.15      0.15      dc         vc
$      sfs       sfm        sst        mst        sfst        sfmt        fsf        vsf
$
$$$$$$$$ contact between workpiece and holder
$
*CONTACT_SURFACE_TO_SURFACE
$      ssid       msid       sstyp       mstyp       sboxid       mboxid       spr         mpr
$            1         3         3         3         vdc          penchk       bt          dt
$      0.15      0.15      dc         vc
$      sfs       sfm        sst        mst        sfst        sfmt        fsf        vsf
$
$$$$$$$$ contact between workpiece and die
$
*CONTACT_SURFACE_TO_SURFACE
$      ssid       msid       sstyp       mstyp       sboxid       mboxid       spr         mpr
$            1         4         3         3         vdc          penchk       bt          dt
$      0.15      0.15      dc         vc
$      sfs       sfm        sst        mst        sfst        sfmt        fsf        vsf
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
```


***CONTROL_CONTACT**
Hemispherical Punch

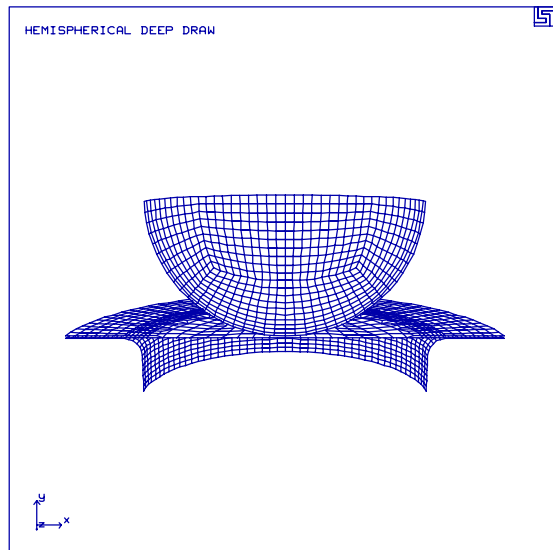
```
1597  0.000000E+00  -5.000533E-01  -7.462286E+01  7  7
1598  0.000000E+00  -5.000534E-01  -7.771143E+01  7  7
1599  0.000000E+00  -5.000535E-01  -8.080000E+01  7  7
$
$$$$$$$ SHELL ELEMENTS
$
*ELEMENT_SHELL
$  eid      pid      n1      n2      n3      n4
   1         1         1         8         9         2
   2         1         2         9        10         3
   3         1         3        10        11         4
   .
   ... in total, 1452 shells defined
   .
1450         4      1589      1596      1597      1590
1451         4      1590      1597      1598      1591
1452         4      1591      1598      1599      1592
*END
```

*CONTROL_CONTACT

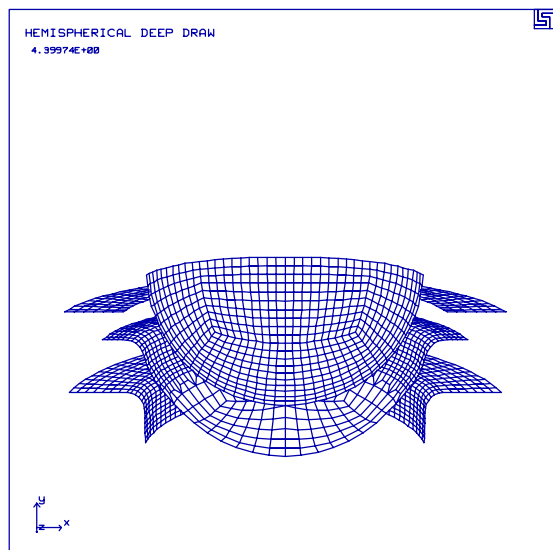
Hemispherical Punch

Results:

taurus g=d3plot
19
rx 10 rayz view



restore rx 10 state 23 explode 1 0 -20 0 1
explode 1 0 10 0 3
explode 1 0 20 0 4 rayz view



LS-DYNA Manual Section: *CONTROL_DAMPING

Additional Sections:

*DAMPING_GLOBAL
*DATABASE_CROSS_SECTION_SET
*LOAD_NODE_SET

Example: Cantilever Beam

Filename: control_damping.beam.k

Description:

A cantilever beam is subjected to a load at the free end. The beam then vibrates relative to the equilibrium position without damping in case 1 and with damping in case 2.

Model:

The beam measures $1000 \times 100 \times 10 \text{ mm}^3$ and is modeled by 10 Belytschko-Tsay shell elements. A force of 100 N is applied in the z-direction at the free end. The calculation ends at 0.5 seconds.

Input for the undamped system:

The force at the free end is applied as two point forces. The size of these forces is controlled by load curve definition number 1 (*DEFINE_CURVE, *LOAD_NODE_SET). The ASCII-files contain information for section force data, nodal information, and shell element information. Data from ASCII-files can be processed in phase 3 of LS-TAURUS.

Input for the damped system:

The same input as in the undamped case except for a global damping constant (*DAMPING_GLOBAL, *CONTROL_DAMPING).

Reference:

Schweizerhof, K. and Weimer, K.

***CONTROL_DAMPING**
Cantilever Beam

```

4
$
*CONTROL_OUTPUT
$  npopt   neecho   nrefup   iaccop   opifs   ipnint   ikedit
    0       0       0       0       0       2       1000
$
*DATABASE_EXTENT_BINARY
$  neiph   neips   maxint   strflg   sigflg   epsflg   rltflg   engflg
    1             1
$  cmpflg   ieverp   beamip
$
*DATABASE_BINARY_D3PLOT
$    dt      lcdt
    0.020
$
*DATABASE_BINARY_D3THDT
$    dt      lcdt
    999999
$
*DATABASE_ELOUT
$    dt
    0.001
$
*DATABASE_HISTORY_SHELL
$   id1     id2     id3     id4     id5     id6     id7     id8
    1
$
*DATABASE_GLSTAT
$    dt
    0.001
$
*DATABASE_NODOUT
$    dt
    0.001
$
*DATABASE_HISTORY_NODE
$   id1     id2     id3     id4     id5     id6     id7     id8
    21
$
*DATABASE_SECFORC
$    dt
    0.001
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Cross Sections
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  define a cross section through the beam to monitor force & moment
$
*DATABASE_CROSS_SECTION_SET
$   nsid    hsid    bsid    ssid    tsid    dsid
    1             1
$
*SET_NODE_LIST
$   sid    da1    da2    da3    da4
    1
$   nid1   nid2   nid3   nid4   nid5   nid6   nid7   nid8
    1       2
$

```

***CONTROL_DAMPING**
Cantilever Beam

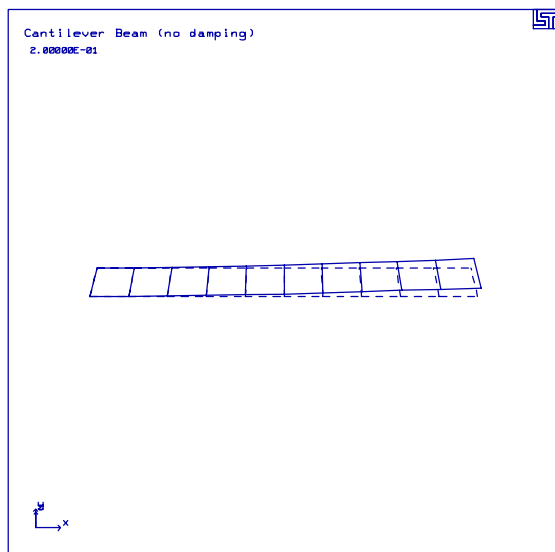
```
$
$$$$ Nodes 1 and 2 have fixed boundary conditions (translation and rotation).
$
*NODE
$  node          x          y          z          tc          rc
   1  0.000000E+00  0.000000E+00  0.000000E+00    7          7
   2  0.000000E+00  1.000000E+02  0.000000E+00    7          7
   3  1.000000E+02  0.000000E+00  0.000000E+00    0          0
   .
   ... in total, 22 nodes defined
   .
  20  9.000000E+02  1.000000E+02  0.000000E+00    0          0
  21  1.000000E+03  0.000000E+00  0.000000E+00    0          0
  22  1.000000E+03  1.000000E+02  0.000000E+00    0          0
$
$$$$$ Shell Elements
$
*ELEMENT_SHELL
$  eid          pid          n1          n2          n3          n4
   1           1           1           3           4           2
   2           1           3           5           6           4
   3           1           5           7           8           6
   4           1           7           9          10           8
   5           1           9          11          12          10
   6           1          11          13          14          12
   7           1          13          15          16          14
   8           1          15          17          18          16
   9           1          17          19          20          18
  10           1          19          21          22          20
$
*END
```

*CONTROL_DAMPING

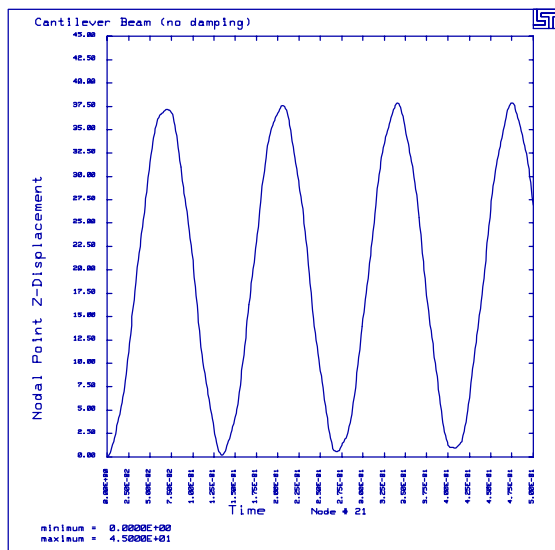
Cantilever Beam

Results:

taurus g=d3plot
rx -40 head Cantilever Beam (no damping)
time 0.2 udg 1 view

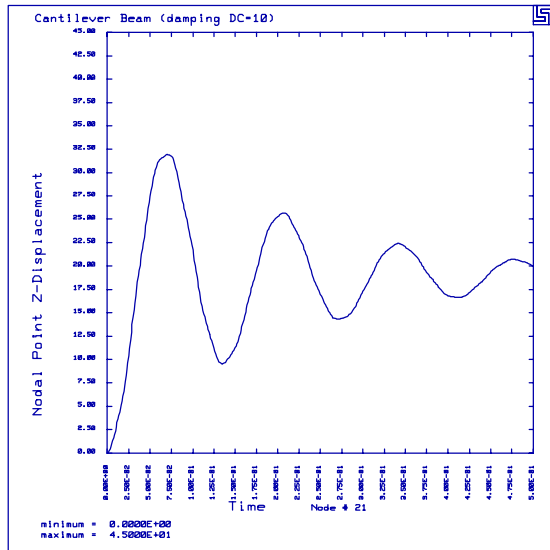


phs3 nodout
head Cantilever Beam (no damping)
oset 0 45 z-disp

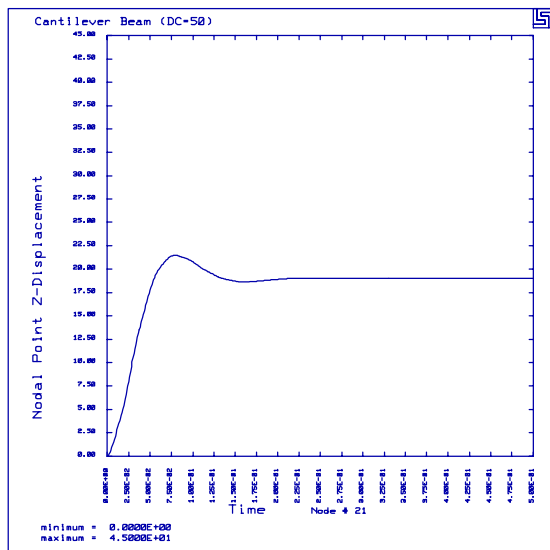


Results:

from phase 3, nodout - damping of DC = 10



from phase 3, nodout - damping of DC = 50



***CONTROL_DAMPING**
Cantilever Beam

LS-DYNA Manual Section: *CONTROL_ENERGY

Example: Bar Impact

Filename: control_energy.bar-impact.k

Description:

A copper bar strikes a wall.

Model:

A 1/4 symmetry bar measures 0.32 cm in radius and 3.24 cm in length and contains 972 hexahedron element. The bar starts at 0.0227 cm/ μ sec and stops at 0 cm/ μ sec. The calculation illustrates the energy balance where $E = KE + IE + HGE$.

Input:

The hourglass energy is computed at a negligible cost. (*CONTROL_ENERGY) The initial velocity for every node is set to -0.0227 except the nodes at $z = 0$.

Results:

The undeformed and deformed shape of the bar are shown. The total, kinetic, internal and hourglass energies are also shown.

*CONTROL_ENERGY

Bar Impact

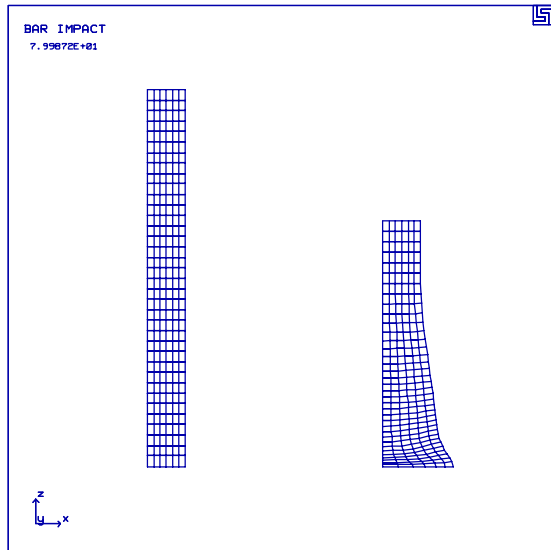
```
$
*ELEMENT_SOLID
$   eid      pid      n1      n2      n3      n4      n5      n6      n7      n8
    1         1         8         1         2         9         45        38        39        46
    2         1         9         2         3        10        46        39        40        47
    3         1        10         3         4        11        47        40        41        48
    .
    ... in total, 972 solids defined
    .
    970         1    1317    1318    1327    1330    1354    1355    1364    1367
    971         1    1330    1327    1328    1331    1367    1364    1365    1368
    972         1    1331    1328    1329    1332    1368    1365    1366    1369
$
*END
```

Results:

taurus g=d3plot

19

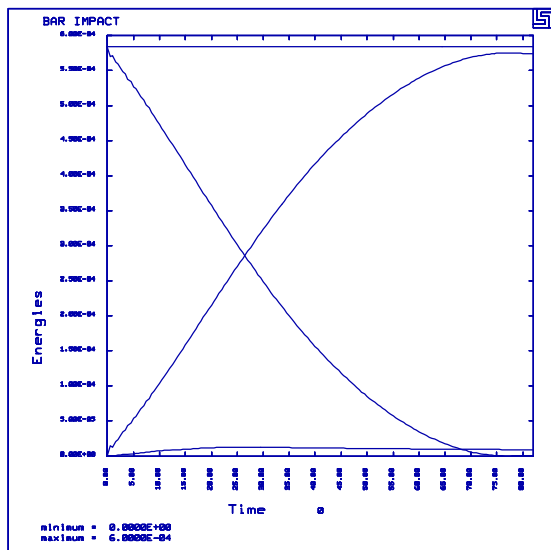
rx -90 angle 1 xtrans -1 view xtrans 2 state 17 over view



phs3 glstat

oset 0 6e-4 otxt Energies

total over kine over inter over hour



***CONTROL_ENERGY**

Bar Impact

LS-DYNA Manual Section: *CONTROL_SHELL

Example: Hemispherical Load

Filename: control_shell.hemi-load.k

Description:

A spherical shell is subjected to outward point loads on the x-axis and inward point loads on the z-axis.

Model:

The 1/8 symmetry model of a sphere measures 10 inches in radius with a thickness of 0.04 inches. The model contains 48 shell elements. A force of one pound is applied in the positive x-direction to the node on the x-axis. A force of one pound is applied in the negative z-direction to the node on the y-axis.

Input:

The element formulation is the Hughes-Liu shell with four integration points through the thickness. Note: If B-T element formulation is used the solution would be incorrect. To fix it, the Belytschko Tsay shell requires the Belytschko-Wang-Chiang warpage stiffness modification (*CONTROL_SHELL). The concentrated loads are applied to two nodes (*DEFINE_CURVE, *LOAD_NODE_POINT).

Results:

The oscillation of the node on the z-axis shows a regular oscillatory behavior. Since there is no specified damping, oscillations would be expected.

Reference:

Belytschko, T., Wang and Chiang.

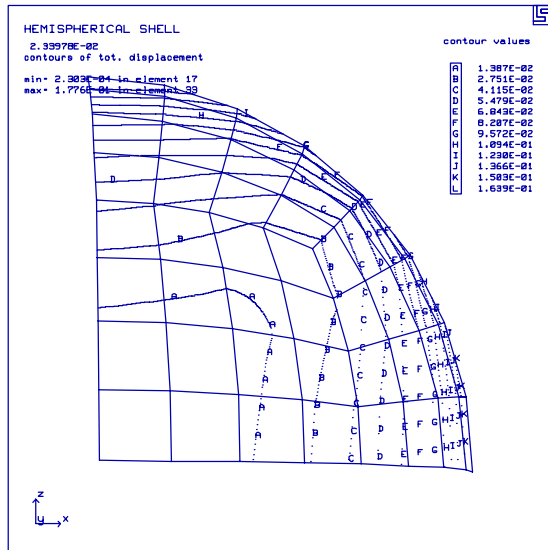
*CONTROL_SHELL

Hemispherical Load

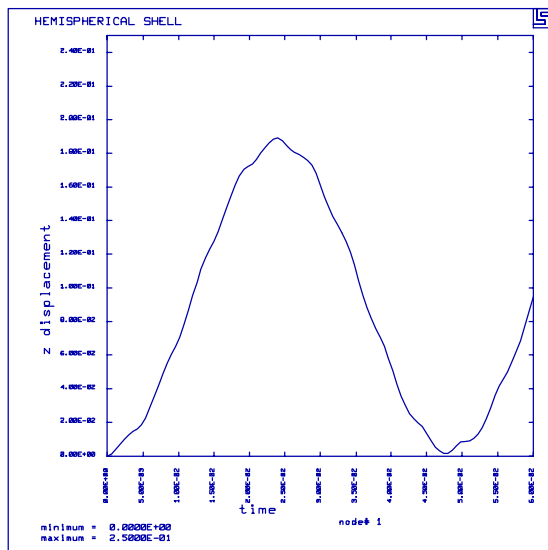
```
.
... in total, 39 nodes defined
.
37  0.000000E+00  -5.500000E-01  1.200000E+01  0  0
38  0.000000E+00   0.000000E+00  1.200000E+01  0  0
39  0.000000E+00   5.500000E-01  1.200000E+01  0  0
$
$$$$$ Shell Elements
$
*ELEMENT_SHELL
$  eid      pid      n1      n2      n3      n4
   1         1         1         4         5         2
   2         1         2         5         6         3
.
... in total, 24 shells defined
.
23         1        34        37        38        35
24         1        35        38        39        36
$
*END
```

Results:

taurus g=d3plot
 19
 rx -90 angle 5 mono numc s 40 contour 20



phs2
 nodes 2 1 10 gather
 oset 0 0.25 black ntime 3 1 1



***CONTROL_SHELL**
Hemispherical Load

LS-DYNA Manual Section: *CONTROL_SHELL

Example: Twisted Cantilever Beam

Filename: control_shell.beam-twist.k

Description:

A beam twisted 90 degrees about its length is constrained on one edge and has a point load prescribed normal to the opposite end of the beam.

Model:

The beam measures $12.00 \times 1.10 \times 0.32$ cubic inches. A concentrated load is applied to one node on the end in the x-direction and the other node on the end in the z-direction.

Input:

This model uses the Hughes-Liu five through the thickness integration points (*CONTROL_SHELL, *SECTION_SHELL). The element has the shell normal update calculation performed at each nodal fiber every cycle (*CONTROL_SHELL). Note: This is another example that will not work correctly with the B-T shell formulation (unless warping stiffness is added).

Results:

The beam oscillates about a neutral amplitude.

Reference:

Belytschko, Wang and Chiang.

*CONTROL_SHELL Twisted Cantilever Beam

```

1
$          abscissa          ordinate
          0.000E+00          1.000E+00
          1.000E+00          1.000E+00
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*PART
$   pid      sid      mid      eosid      hgid      adpopt
Hemisphere
          1          1          1
$
$
$
*MAT_PLASTIC_KINEMATIC
$   mid      ro      e      pr      sigy      etan      beta
          1 1.000E-03 6.825E+07      0.3 600000.00 0.000E+00 0.000E+00
$   src      srp      fs
          0.000E+00 0.000E+00 0.000E+00
$
$
$
*SECTION_SHELL
$   sid      elform      shrif      nip      propt      qr/irid      icomp
          1          .          .          5
$   t1      t2      t3      t4      nloc
          4.000E-02 4.000E-02 4.000E-02 4.000E-02
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Nodes and Elements
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Multiple nodes have boundary conditions to simulate symmetry.
$
*NODE
$   node      x      y      z      tc      rc
          1 0.000000E+00 0.000000E+00 1.000000E+01 1 5
          2 1.950897E+00 0.000000E+00 9.807854E+00 0 0
          3 3.826834E+00 0.000000E+00 9.238795E+00 0 0
          .
          ... in total, 61 nodes defined
          .
          59 8.180990E+00 1.705178E+00 5.492155E+00 0 0
          60 7.794079E+00 3.370117E+00 5.281538E+00 0 0
          61 7.167934E+00 4.930554E+00 4.930554E+00 0 0
$
$$$$$ Shell Elements
$
*ELEMENT_SHELL
$   eid      pid      n1      n2      n3      n4
          1          1          1          6          7          2
          2          1          2          7          8          3
          3          1          3          8          9          4
          .
          ... in total, 48 shells defined

```

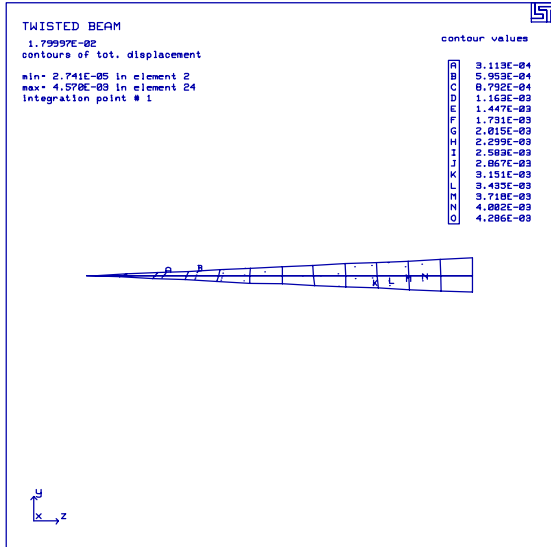
***CONTROL_SHELL**
Twisted Cantilever Beam

.					
46	1	59	10	15	60
47	1	60	15	20	61
48	1	61	20	25	45

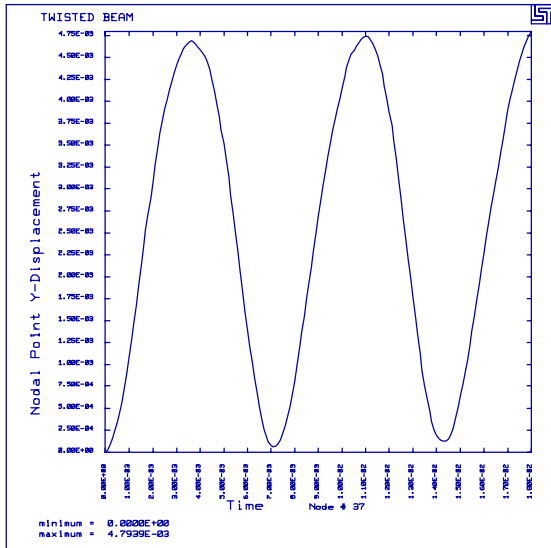
\$
*END

Results:

taurus g=d3plot
19
ry 90 state 19 mono numc 15 contour 20



phs3
nodout
black y-disp



***CONTROL_SHELL**
Twisted Cantilever Beam

LS-DYNA Manual Section: *CONTROL_TIMESTEP

Example: Billet Upset

Filename: control_timestep.billet-forge.k

Description:

A rod of steel is forged between two dies. The billet upset problem is a measure of friction under forming conditions.

Model:

The billet material is isotropic elastic-plastic, and the model has 1/8 symmetry. The billet measures 2.25 inches in height and 1.26 inches in radius. The die compresses the billet 1.60 inches. The relationship between the shear friction and the normal pressure is bilinear.

Input:

The mass scaling time step size is set to 12 microseconds (*CONTROL_TIMESTEP). The billet nodes contact the die surfaces (*CONTACT_NODES_TO_SURFACE). The Coulomb frictional constant is 0.10 and the constant shear is 2,055 psi . A half sine wave defines the velocity of the die (*BOUNDARY_PRESCRIBED_MOTION).

Results:

The results show that effective plastic strains with and without timestep control are the same. CPU savings is approximately 33% on the cray J90 using 1 cpu..

Reference:

Avitzur, B., Lee, C. H. and Altan, T.

***CONTROL_TIMESTEP**
Billet Upset

```
$      dt
  0.00001
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Loading - PRESCRIBED_MOTION_RIGID
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
*BOUNDARY_PRESCRIBED_MOTION_RIGID
$      mid      dof      vad      lcid      sf      vid
      2         3         0         1 1.000E+00
$
*DEFINE_CURVE
$      lcid      sidr      scla      sclo      offa      offo
      1
$      abscissa      ordinate
      0.000E+00      0.000E+00
      5.000E-05      -4.931E+00
      1.000E-04      -1.960E+01
      1.500E-04      -4.365E+01
      2.000E-04      -7.649E+01
      2.500E-04      -1.173E+02
      3.000E-04      -1.651E+02
      3.500E-04      -2.187E+02
      4.000E-04      -2.767E+02
      4.500E-04      -3.378E+02
      5.000E-04      -4.005E+02
      5.500E-04      -4.632E+02
      6.000E-04      -5.243E+02
      6.500E-04      -5.823E+02
      7.000E-04      -6.359E+02
      7.500E-04      -6.837E+02
      8.000E-04      -7.245E+02
      8.500E-04      -7.573E+02
      9.000E-04      -7.814E+02
      9.500E-04      -7.961E+02
      1.000E-03      -8.010E+02
      1.050E-03      -7.961E+02
      1.100E-03      -7.814E+02
      1.150E-03      -7.573E+02
      1.200E-03      -7.245E+02
      1.250E-03      -6.837E+02
      1.300E-03      -6.359E+02
      1.350E-03      -5.823E+02
      1.400E-03      -5.243E+02
      1.450E-03      -4.632E+02
      1.500E-03      -4.005E+02
      1.550E-03      -3.378E+02
      1.600E-03      -2.767E+02
      1.650E-03      -2.187E+02
      1.700E-03      -1.651E+02
      1.750E-03      -1.173E+02
      1.800E-03      -7.649E+01
      1.850E-03      -4.365E+01
      1.900E-03      -1.960E+01
      1.950E-03      -4.931E+00
      2.000E-03      0.000E+00
      2.200E-03      0.000E+00
$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
```


***CONTROL_TIMESTEP**
Billet Upset

```

*SECTION_SHELL
$   sid   elform   shrf   nip   propt   qr/irid   icomp
    2
$   t1     t2     t3     t4     nloc
 1.000E-02 1.000E-02 1.000E-02 1.000E-02
$
$
$$$$$ Define Nodes and Elements
$
$$$$$ Many nodes have boundary conditions in order to simulate symmetry.
$
*NODE
$   node          x          y          z          tc          rc
    1   0.000000E+00  0.000000E+00  0.000000E+00    7          7
    2   4.687500E-02  0.000000E+00  0.000000E+00    5          7
    3   9.375000E-02  0.000000E+00  0.000000E+00    5          7
    .
    ... in total, 5755 nodes defined
    .
 5753   9.731613E-01  8.317921E-01  1.126000E+00    0          0
    .
 5754   1.018930E+00  8.704337E-01  1.126000E+00    0          0
 5755   1.064698E+00  9.090752E-01  1.126000E+00    0          0
$
$$$$$ Solid Elements
$
*ELEMENT_SOLID
$   eid   pid   n1   n2   n3   n4   n5   n6   n7   n8
    1     1     1    2   11   10   82   83   92   91
    2     1     2    3   12   11   83   84   93   92
    3     1     3    4   13   12   84   85   94   93
    .
    ... in total, 4576 solids defined
    .
 4574     1   5307  5308  3627  3618  5379  5380  3708  3699
 4575     1   5308  5309  3636  3627  5380  5381  3717  3708
 4576     1   5309  5310  3645  3636  5381  5382  3726  3717
$
$$$$$ Shell Elements
$
*ELEMENT_SHELL
$   eid   pid   n1   n2   n3   n4
    1     2   5383  5394  5395  5384
    2     2   5384  5395  5396  5385
    3     2   5385  5396  5397  5386
    .
    ... in total, 340 shells defined
    .
 338     2   5752  5602  5613  5753
 339     2   5753  5613  5624  5754
 340     2   5754  5624  5635  5755
$
*END

```

*CONTROL_TIMESTEP

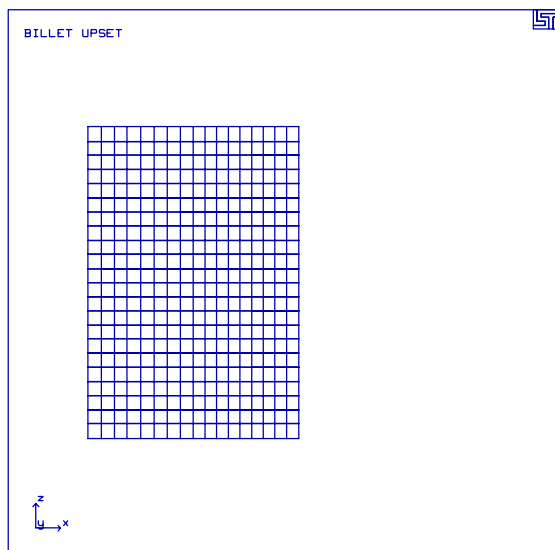
Billet Upset

Results:

taurus g=d3plot

19

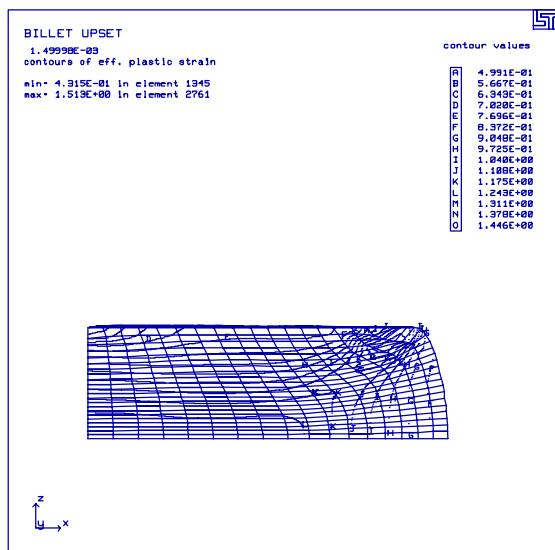
rx -90 angle 5 m 1 view



state 16

numc 15 mono

contour 7



LS-DYNA Manual Section: *CONTROL_ADAPTIVE

Additional Sections:

*DAMPING_GLOBAL
*LOAD_RIGID_BODY

Example: Deep Drawing with Adaptivity

Filename: control_adaptive.cup-draw.k

Description:

This problem includes three tools a punch, a binder and a die and also includes a blank to be formed. The blank is deep drawn by the punch while the binder and die hold the blank edges and help prevent wrinkling. During the process, adaptivity is employed to refine the mesh of the blank to improve accuracy.

Model:

Only 1/4 of the system is modeled because of symmetry. The binder pushes down on the blank against the die using a *LOAD_RIGID command to model the boundary edge condition. The punch is moved down onto the blank with a *BOUNDARY_PRESCRIBED_MOTION_RIGID command. Global damping and contact damping are defined to prevent local nodal vibrations. The time step size is controlled with mass scaling because inertial effects are insignificant in this problem. One way surface to surface contact is defined between the major parts. This allows the drawing (i.e., contact) forces to be monitored using the rforc ascii output file.

Results:

During the drawing operation, the mesh is refined considerably.

*CONTROL_ADAPTIVE Deep Drawing with Adaptivity

```
*DATABASE_BINARY_D3PLOT
$      dt      lcdt
      40.0

$
*DATABASE_GLSTAT
$      dt
      1.0

$
*DATABASE_MATSUM
$      dt
      1.0

$
*DATABASE_RBDOUT
$      dt
      5.0

$
*DATABASE_RCFORC
$      dt
      1.0

$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Adaptivity
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>....1.>....2.>....3.>....4.>....5.>....6.>....7.>....8
$
*CONTROL_ADAPTIVE
$  adpfreq  adptol  adpopt  maxlvl  tbirth  tdeath  lcadp  ioflag
      5.0e+0   0.1     2       2      0.0    0.0     0
$
$
*DAMPING_GLOBAL
$  lcid  valdmp
      3
$
*DEFINE_CURVE
$  lcid  sidr  scla  sclo  offa  offo
      3
$
      abscissa  ordinate
      0.000E+00  0.000E+00
      1.000E+04  0.000E+00
      1.001E+04  3.000E+03
      2.000E+04  3.000E+03
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Loading and Boundary Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>....1.>....2.>....3.>....4.>....5.>....6.>....7.>....8
$
*BOUNDARY_PRESCRIBED_MOTION_RIGID
$  pid  dof  vad  lcid  sf  vid  death
      1   2   0   1    -1.  vid  death
$
*DEFINE_CURVE
$  lcid  sidr  scla  sclo  offa  offo
      1
$
      abscissa  ordinate
```

***CONTROL_ADAPTIVE**
Deep Drawing with Adaptivity

0.000E+00	0.000E+00
1.000E+02	2.912E-03
2.000E+02	5.540E-03
3.000E+02	7.625E-03
4.000E+02	8.963E-03
5.000E+02	9.425E-03
6.000E+02	8.963E-03
7.000E+02	7.625E-03
8.000E+02	5.540E-03
9.000E+02	2.912E-03
1.000E+03	0.000E+00

```
$
$ From a sheet metal forming example. A blank is hit by a punch, a binder is
$ used to hold the blank on its sides. The rigid holder (part 2) is held
$ against the blank using a load applied to the cg of the holder.
$
$ The direction of the load is in the y-direction (dof=2) but is scaled
$ by sf = -1 so that the load is in the correct direction. The load
$ is defined by load curve 2.
```

```
$
$ *LOAD_RIGID_BODY
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$ pid dof lcid sf cid m1 m2 m3
$ 2 2 2 -1.0
```

```
$
$ *DEFINE_CURVE
$ lcid sidr scla sclo offa offo
$ 2
$ abscissa ordinate
$ 0.000E+00 8.000E-05
$ 1.000E+04 8.000E-05
```

\$\$\$\$ Define Parts and Materials

```
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
```

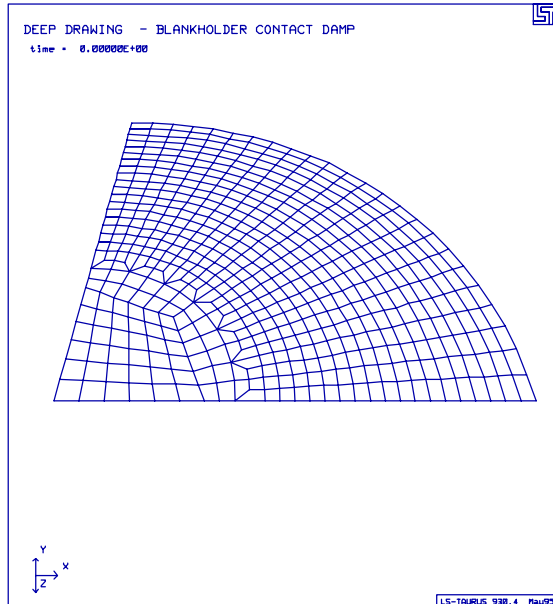
```
$
$ *PART
$ pid sid mid eosid hgid grav adpopt
punch
$ 1 1 2 0 0 0 0
binder
$ 2 1 2 0 0 0 0
blank
$ 3 1 1 0 0 0 1
die
$ 4 1 2 0 0 0 0
```

```
$
$ *MAT_PLASTIC_KINEMATIC
$ mid ro e pr sigy etan beta
$ 1 2.700E+00 0.690E+00 3.000E-01 8.180E-04 0.010E+00 1.000E+00 0.000E+00
$ src srp fs
$ 0.000E+00 0.000E+00
```

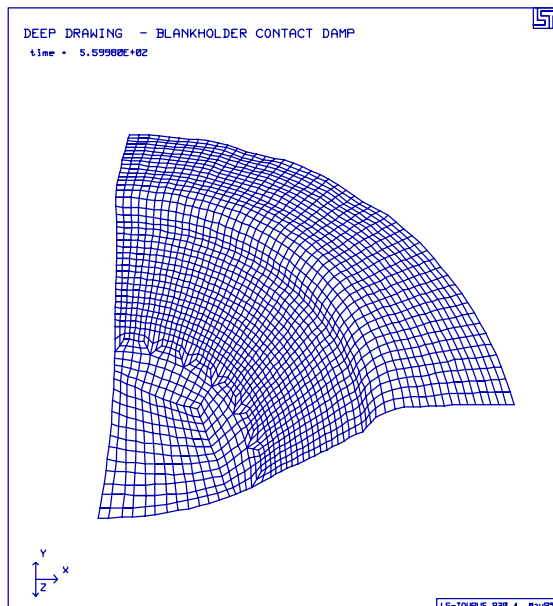
```
$
$ *MAT_RIGID
$ mid ro e pr n couple m alias
```


Results:

taurus g=d3plot
rx 45 m 3 s 15 center
state 1 view



state 15
view



LS-DYNA Manual Section: *CONTROL_ADAPTIVE

Additional Sections:

*CONTROL_SUBCYCLE

Example: Square Crush Tube with Adaptivity

Filename: control_adaptive.square-beam.k

Description:

A square cross section of a crush tube uses adaptivity to re-fine the mesh as needed to improve accuracy..

Model:

Only 1/4 of the tube is modeled because of symmetry. The nodes on top of the crush tube are assigned extra mass with *ELEMENT_MASS and given an initial velocity in the y-direction of -5,646 mm/s. The nodes on the bottom of the tube are fixed in y-translation. Automatic single surface contact is defined to prevent penetration when the folds of the crush tube start to form. The model has subcycling defined.

Results:

The mesh at the fold location in the crush tube is automatically re-fined as the crush progresses.

***CONTROL_ADAPTIVE**
Square Crush Tube with Adaptivity

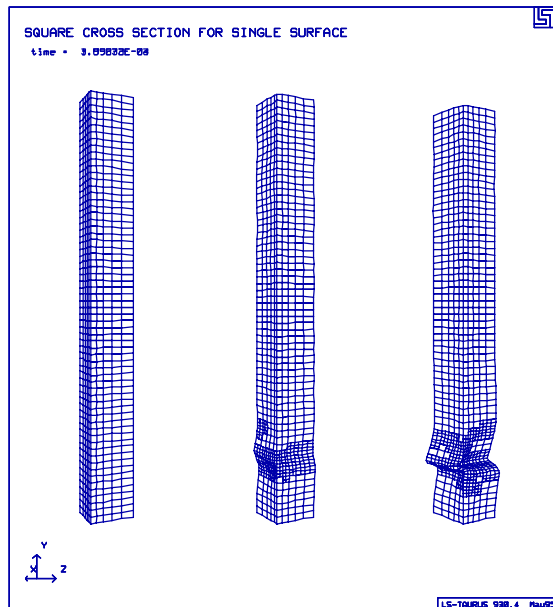
```
$
*ELEMENT_MASS
$   eid      nid      mass
    65      65      1.000E-02
    66      66      1.000E-02
    99      99      1.000E-02
   132     132      1.000E-02
   165     165      1.000E-02
   198     198      5.000E-03
   423     423      1.000E-02
   456     456      1.000E-02
   489     489      1.000E-02
   522     522      1.000E-02
   555     555      5.000E-03
$
*END
```

*CONTROL_ADAPTIVE

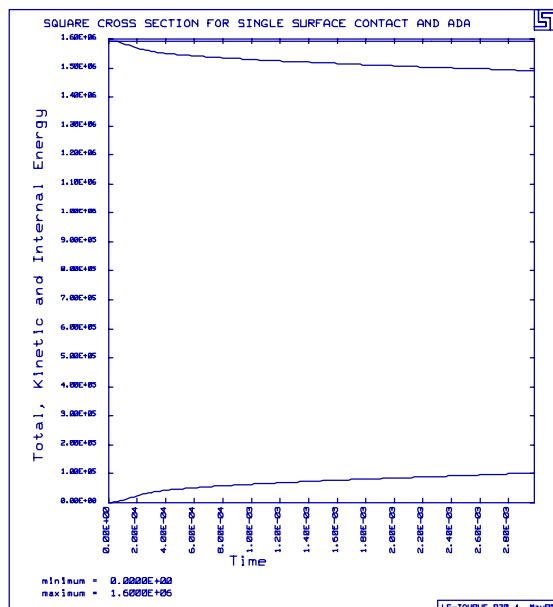
Square Crush Tube with Adaptivity

Results:

taurus g=d3plot
ry 120 xtran -150 v xtran 150 s 5 over v
xtran 150 s 20 over v



phs3 glstat
otxt Total, Kinetic and Internal Energy
oset 0 1.6e6 total over kine over inte



LS-DYNA Manual Section: *CONTROL_ADAPTIVE

Additional Sections:

*DEFINE_COORDINATE_VECTOR

Example: Cylinder Undergoing Deformation with Adaptivity

Filename: control_adaptive.cylinder.k

Description:

Several nodes on a cylinder are given initial velocities towards the center of the cylinder causing the cylinder to indent. To improve accuracy, adaptivity is defined so that the mesh of the cylinder is re-fined during the deformation.

Model:

Only 1/4 of the system is modeled because of symmetry. The boundary conditions on the cylinder are defined with single point constraints (SPC's). Because of the geometry orientation, several of the SPC's require local coordinate system defined using the keyword *DEFINE_COORDINATE_VECTOR.

Results:

Before and after mesh refinement are shown in the figures. Additionally, the total, kinetic and internal energy from the glstat ascii file are shown. The entire initial kinetic energy is absorbed by the cylinder due to material deformation (internal energy).

*CONTROL_ADAPTIVE

Cylinder Undergoing Deformation with Adaptivity

List of LS-DYNA input deck:

```

*KEYWORD
*TITLE
ADAPTIVITY: circular cylinder (8x16)
$
$  LSTC Example
$
$  Last Modified: October 14, 1997
$
$  Units: lbf-s2/in, in, s, lbf, psi, lbf-in
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONTROL_TERMINATION
$  endtim  endcyc  dtmin  endeng  endmas
  0.0004
$
*CONTROL_ENERGY
$    hgen     rwen    slnten   ryles
    2         2
$
*CONTROL_OUTPUT
$  npopt  neecho  nrefup  iaccop  opifs  ipnint  ikedit
    1         3
$
*CONTROL_SHELL
$  wrpang  itrist   irnxx   istupd   theory  bwc    miter
                           1         2         1
$
$
*DATABASE_BINARY_D3PLOT
$    dt      lcdt
  0.00002
$
*DATABASE_GLSTAT
$    dt
  0.00002
$
*DATABASE_MATSUM
$    dt
  0.00002
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Adaptivity
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONTROL_ADAPTIVE
$  adpfreq  adptol  adpopt  maxlvl  tbirth  tdeath  loadp  ioflag
   1.01e-5   10.0    2        3       0.0     0.0     0       1
$
$

```

*CONTROL_ADAPTIVE

Cylinder Undergoing Deformation with Adaptivity

```

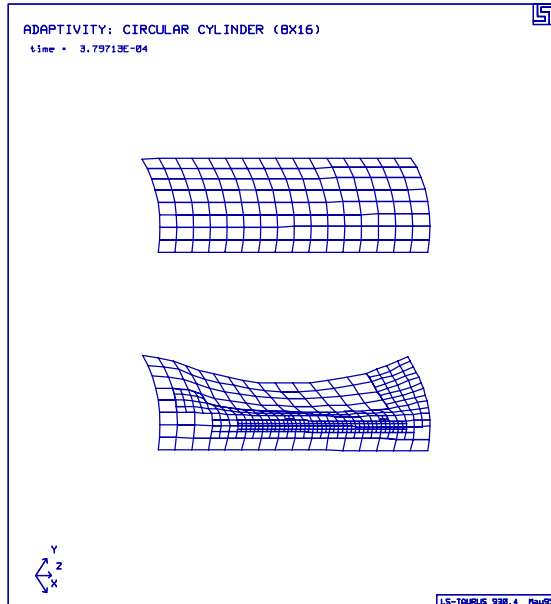
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*PART
$   pid      sid      mid      eosid      hgid      grav      adpopt
al6061-t6
    1        1        1        0          0          0          1
$
$
*MAT_PLASTIC_KINEMATIC
$   mid      ro      e      pr      sigy      etan      beta
    1 2.500E-04 1.050E+07 3.300E-01 4.400E+04 0.000E+00 1.000E+00
$
$   src      srp      fs
    0.000E+00 0.000E+00
$
$
*SECTION_SHELL
$   sid      elform      shrf      nip      propt      qr/irid      icomp
    1        2          1.       5.       0.        0.          0
$   t1      t2      t3      t4      nloc
    0.125    0.125    0.125    0.125
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Boundary Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*BOUNDARY_SPC
$   nid      cid      dofz      dofry      dofz      dofry      dofz      dofry      dofz
    1        1        1          1          0          0          1          1
    18       2        0          1          0          0          1          1
    35       3        0          1          0          0          1          1
.
... in total, 48 SPC's defined
.
    68       4        1          1          0          0          1          1
    85       5        1          1          0          0          1          1
    102      6        1          1          0          0          1          1
    119      7        1          1          0          0          1          1
    120      8        0          1          0          0          1          1
    153      1        1          1          1          1          1          1
$
$
*DEFINE_COORDINATE_VECTOR
$   cid      xx      yx      zx      xv      yv      zv
    1        1.      0.      0.      0.      1.      0.
    2  0.99144 -0.13053 0.00000 0.13053 0.99144 0.00000
    3  0.96593 -0.25882 0.00000 0.25882 0.96593 0.00000
    4  0.92388 -0.38268 0.00000 0.38268 0.92388 0.00000
    5  0.86603 -0.50000 0.00000 0.50000 0.86603 0.00000
    6  0.79335 -0.60876 0.00000 0.60876 0.79335 0.00000
    7  0.70711 -0.70711 0.00000 0.70711 0.70711 0.00000
    8  0.60876 -0.79335 0.00000 0.79335 0.60876 0.00000
    9  0.50000 -0.86603 0.00000 0.86603 0.50000 0.00000

```

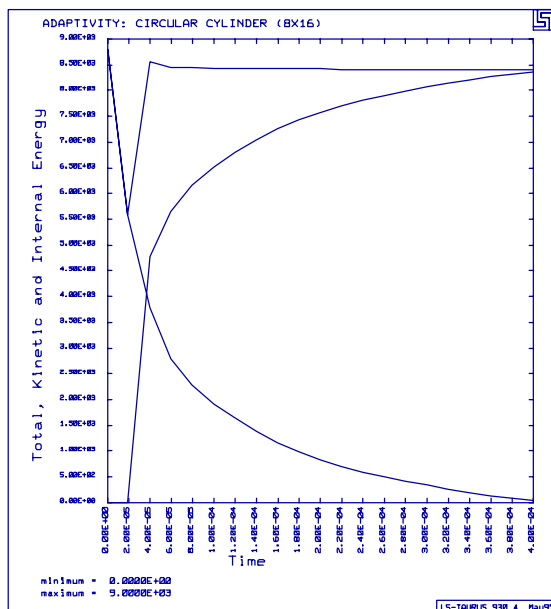

*CONTROL_ADAPTIVE Cylinder Undergoing Deformation with Adaptivity

Results:

taurus g=d3plot
angle 1 ry 90 rx -45 ry -45 ytrans 3 view
ytrans -6 s 20 over view



phs3 glstat
otxt Total, Kinetic and Internal Energy
oset 0 9e3 total over kine over inte



***CONTROL_ADAPTIVE**

Cylinder Undergoing Deformation with Adaptivity

LS-DYNA Manual Section: *DAMPING_GLOBAL

Additional Sections:

*CONTROL_DAMPING
*LOAD_BODY_Z

Example: Tire Bounces on the Ground and Damps Out

Filename: damping.tire.k

Description:

A simple model of a tire is placed under gravity loading and drops onto rigid solid elements. Fully integrated shell elements are used for the tire to prevent hourglassing from damping out the model. Additionally, rigid solid elements are used for modeling the ground instead of a rigidwall because the rigidwall will also damp the system because of its' perfectly plastic contact definition. Thus, to damp out the bouncing, global damping is applied to the system.

Model:

Global damping of 0.5 is applied to the system using the *DAMPING_GLOBAL keyword. Contact between the tire and ground is defined using node to surface contact. Gravity is applied with the *LOAD_BODY_Z command.

Results:

The total energy of the system comes from the external energy of gravity (potential energy of "mgh"). This energy is absorbed by the damping in the model.

***DAMPING_GLOBAL**
Tire Bounces on the Ground and Damps Out

```

      .
      ... in total, 1522 nodes defined
      .
      52040 2.444749625E+02 -7.51864725E+02 -2.79200000E+02
      52049 2.698749875E+02 -7.51864725E+02 -2.79200000E+02
$
$$$$$$$$$$$$ Shell Elements
$
*ELEMENT_SHELL
$   eid      pid      n1      n2      n3      n4
    8710      35      8719      8722      8723      8720
      .
      ... in total, 96 shells defined
      .
    8949      36      8929      8932      8926      8924
$
$$$$$$$$$$$$ Solid Elements
$
*ELEMENT_SOLID
$   eid      pid      n1      n2      n3      n4      n5      n6      n7      n8
    50880      76      50315      52520      52902      52521      52362      52686      52950      52687
      .
      ... in total, 534 solids defined
      .
    51588      76      53833      53962      53834      53423      53424      53835      53425      53689
$
$$$$$$$ Nodal Mass Elements
$
*ELEMENT_MASS
$   eid      nid      mass
    8730      8730      10.0
    8746      8746      10.0
$
*END

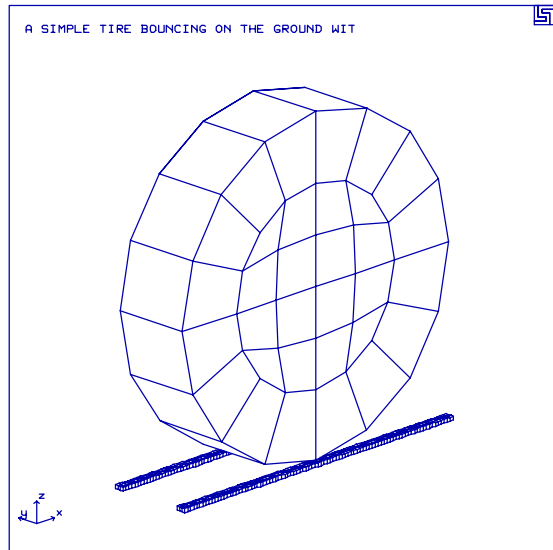
```

*DAMPING_GLOBAL

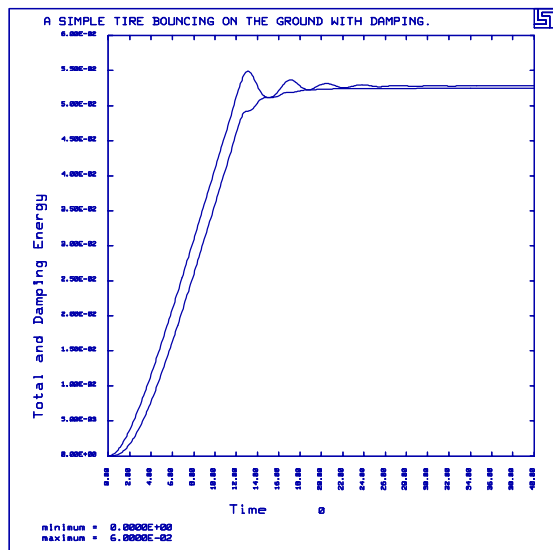
Tire Bounces on the Ground and Damps Out

Results:

taurus g=d3plot
angle 1 rx -90
ry 45 rx 20 view



phs3 glstat
otxt Total and Damping Energy
oset 0 0.06 total over damping



LS-DYNA Manual Section: *DEFORMABLE_TO_RIGID

Additional Sections:

*BOUNDARY_SPC_NODE
*LOAD_BODY_Y
*RIGID_DEFORMABLE_R2D

Example: Interaction of Pendulums

Filenames: deformable_to_rigid.pendulum.k
deformable_to_rigid.pendulum.res

Execution lines:

```
ls940 i= deformable_to_rigid.pendulum.k  
ls940 i= deformable_to_rigid.pendulum.res r=d3dump01
```

Description:

Two spheres are connected to wires to form two pendulums. One sphere is in a horizontal position with gravitational acceleration, base acceleration and is given an initial velocity in the vertical direction. The other sphere is in the vertical direction. The spheres are treated as rigid bodies while no contact or deformation occurs (i.e., when the horizontal pendulum swings down towards the vertical pendulum). The spheres are switched to deformable through a restart file so that they become flexible during contact.

Model:

Both spheres are modeled using shell elements. The pendulum wires are modeled using elastic beams. Automatic single surface contact is used during the impact phase.

Reference:

Reid, J.D.

***DEFORMABLE_TO_RIGID**

Interaction of Pendulums

```

$
$$$$ Boundary and Initial Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>....1.>....2.>....3.>....4.>....5.>....6.>....7.>....8
$
$$$$ Constrain translation of end points of beams
$
*BOUNDARY_SPC_NODE
$
    nid          cid          dofx          dofy          dofz          dofrx          dofry          dofrz
    45004          0           1           1           1           0           0           0
    45005          0           1           1           1           0           0           0
    45010          0           1           1           1           0           0           0
    45011          0           1           1           1           0           0           0
$
$
$$$$ The nodes within box 5 are given an initial velocity.
$
*INITIAL_VELOCITY
$
    nsid          nsidex          boxid
                   5
$
    vx           vy           vz           wx           wy           wz
    0.0          -12.0         0.0
$
*DEFINE_BOX
$
    boxid          xmm          xmx          ymn          ymx          zmn          zmx
    5           -120.0         -80.0         80.0         120.0         -30.0         30.0
$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>....1.>....2.>....3.>....4.>....5.>....6.>....7.>....8
$
$$$$$ SPHERES
$
*PART
$
    pid          sid          mid          eosid          hgid          adpopt
sphere1
    1           1           1
sphere2
    2           2           1
$
$
$$$$$ Materials
$
$ Aluminum
$
*MAT_PLASTIC_KINEMATIC
$
    mid          ro          e          pr          sigy          etan          beta
    1          2.70e-6         68.9         0.330         0.286         0.00689
$
    src          srp          fs
$
$
$$$$$ Sections
$
$
*SECTION_SHELL

```

***DEFORMABLE_TO_RIGID**
Interaction of Pendulums

```

$
$      sid   elform   shrf     nip     propt  qr/irid   icomp
$      1     2         3         4         nloc
$      1.0   1.0     1.0     1.0
$
*SECTION_SHELL
$
$      sid   elform   shrf     nip     propt  qr/irid   icomp
$      2     2         3         4         nloc
$      1.0   1.0     1.0     1.0
$
$
$$$$$  PENDULUM WIRES - ELASTIC BEAMS
$
*PART
$      pid     sid     mid     eosid     hgid     adpopt
Pendulum Wires - Elastic Beams
$      45      45      45
$
$
*MAT_ELASTIC
$      mid     ro       e       pr       da       db       k
$      45     7.86e-6  210.0   0.30
$
$
*SECTION_BEAM
$      sid   elform   shrf   qr/irid   cst
$      45    3     1.00000  1.0
$ res:  a     iss     itt     irr     sa
$      10.0
$
$
$$$$$ Deformable Switching
$
$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*DEFORMABLE_TO_RIGID
$      pid     mrb
$      1
$
*DEFORMABLE_TO_RIGID
$      pid     mrb
$      2
$
$
$$$$$ Define Nodes
$
$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*NODE
$      node          x          y          z          tc          rc
$      1 -1.08660250E+02 9.133975000E+01 -3.66025000E+00

```

*DEFORMABLE_TO_RIGID

Interaction of Pendulums

```
2 -1.09496480E+02 9.331914000E+01 -4.49648000E+00
3 -1.10108300E+02 9.545641000E+01 -5.10830000E+00
.
... in total, 784 nodes defined
.
770 2.654228546E+01 -6.85637234E-01 1.355349000E+01
771 2.563811870E+01 1.747789010E+00 1.314240000E+01
772 2.445826961E+01 3.903858475E+00 1.250087000E+01
45004 5.000000000E+00 1.000000000E+02 -5.00000000E+01
45005 5.000000000E+00 1.000000000E+02 6.000000000E+01
45010 1.500000000E+01 1.000000000E+02 -5.00000000E+01
45011 1.500000000E+01 1.000000000E+02 6.000000000E+01
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$ Extra Nodes for Beams
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
45012 -8.83925000E+01 1.057467600E+02 -7.46760000E-01
45013 9.444594624E+00 8.495260182E+00 -1.11255000E+00
45014 -8.80996038E+01 9.496034978E+01 -7.46760000E-01
45015 1.816524677E+01 8.921481149E+00 -7.46760000E-01
45016 -8.80996068E+01 1.057467600E+02 1.003965322E+01
45017 9.446435484E+00 8.493592403E+00 1.104210976E+01
45018 -8.79698503E+01 9.483059027E+01 1.016940973E+01
45019 1.816697500E+01 8.920056610E+00 1.067986974E+01
$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Elements
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*ELEMENT_BEAM
$   eid      pid      n1      n2      n3
45000      45      350     45004     45012
45001      45      678     45010     45013
45002      45      346     45004     45014
45003      45      681     45010     45015
45004      45      378     45005     45016
45005      45      710     45011     45017
45006      45      374     45005     45018
45007      45      713     45011     45019
$
*ELEMENT_SHELL
$   eid      pid      n1      n2      n3      n4
1          1          1      10      11      2
2          1          2      11      12      3
3          1          3      12      13      4
.
... in total, 768 shells defined
.
766      2      770      643      651      771
767      2      771      651      659      772
768      2      772      659      667      723
$
*END
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
```

***DEFORMABLE_TO_RIGID**
Interaction of Pendulums

```

*KEYWORD
*TITLE
Pendulum with 2 spheres colliding
$
$
$$$$$ Restart
$
$ Last Modified: September 16, 1997
$
$ Units: mm, kg, ms, kN, GPa, kN-mm
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Switch spheres to deformables
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*RIGID_DEFORMABLE_R2D
$      pid
      1
$
*RIGID_DEFORMABLE_R2D
$      pid
      2
$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONTROL_TERMINATION
$      ENDTIM      ENDCYC      DTMIN      ENDENG      ENDMAS
           13.0          0          0.0          0.0          0.0
$
$$$$$ Increase d3plot output frequency to capture deformation of impact better.
$
*DATABASE_BINARY_D3PLOT
$      dt      lcdt
           0.10
$
*END

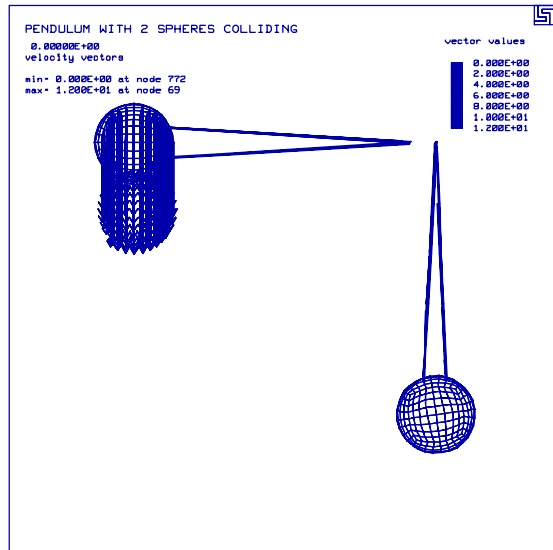
```

*DEFORMABLE_TO_RIGID

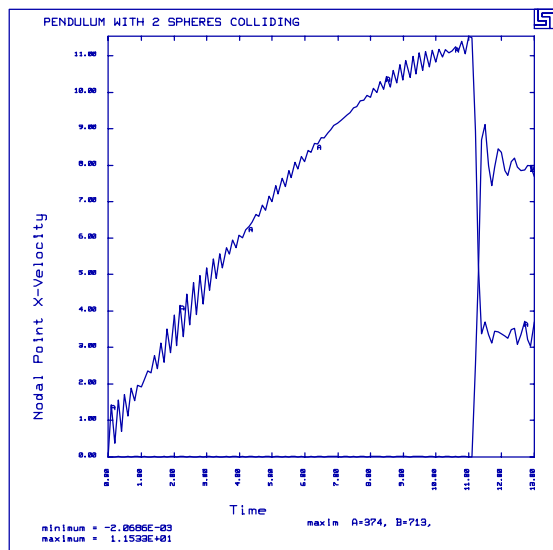
Interaction of Pendulums

Results:

taurus g=d3plot
19
state 1 angle 1 vect v



phs3
nodout
x-vel 374 713



LS-DYNA Manual Section: *INTEGRATION_SHELL

Additional Sections:

*DAMPING_GLOBAL
*LOAD_NODE_POINT

Example: Cantilever Beam with Lobotto Integration

Filename: integration_shell.lobotto.beam.k

Description:

A cantilever beam has a concentrated load, and then the beam vibration critically damps. Lobotto integration rules place the quadrature points on the true surfaces of the shell. [See Hughes].

Model:

The plate measures $1.00 \times 0.10 \times 0.01$ in³ and is modeled with 60 Belytschko-Tsay shell elements. The displacement of the nodes is fixed at one end and a concentrated load is applied to the other end. Symmetry conditions for the plane strain case exist on the beam sides.

Input:

The concentrated loads and load curve definition 1 defines the load on the end of the beam (*LOAD_NODE_POINT, *DEFINE_CURVE). The beam is critically damped (*DAMPING_GLOBAL) The number of integration points is 5 (*SECTION_SHELL). The shell integration rule is the Lobotto integration rule (*SECTION_SHELL)

Results:

The displacement of the beam damps out critically. The x-stress values at the integration points exhibit tension on one side, compression on the opposite side, and balance at the neutral axis.

***INTEGRATION_SHELL**

Cantilever Beam with Lobotto Integration

59	1	60	91	92	61
60	1	61	92	93	62

\$
*END

*INTEGRATION_SHELL

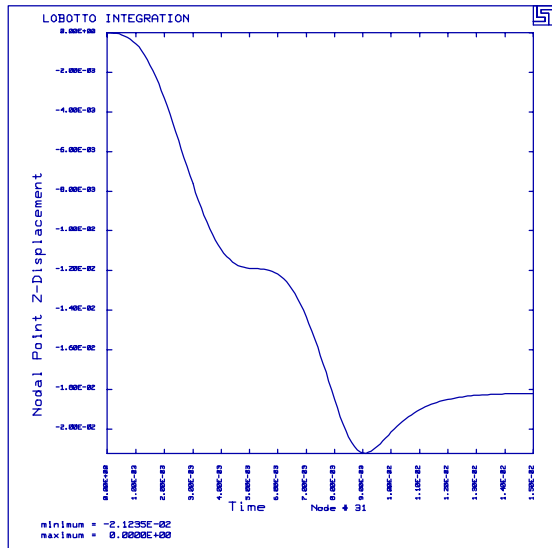
Cantilever Beam with Lobotto Integration

Results:

taurus g=d3plot
19
rx -90 s 50 udg 1 g



phs3
nodout
z-disp



***INTERFACE_COMPONENT**

An Interface File Controls the Response of a Cube

LS-DYNA Manual Section: *INTERFACE_COMPONENT

Additional Sections:

*INITIAL_VELOCITY
*INTERFACE_LINKING_SEGMENT

Example: An Interface File Controls the Response of a Cube

Filenames: interface_component.cube.k
interface_component.cube.rk

Execution Line:

```
LS940 i=interface_component.cube.k z=d3iff
```

After completion, copy d3iff to a separate directory containing interface_component.cube.rk, then from that directory run:

```
LS940 i=interface_component.cube.rk l=d3iff
```

Description:

A cube, one solid element, strikes and rebounds from an elastic plate. In the first run, an interface file (d3iff) is created that contains the position of the bottom segment of the cube. In the second run, the cube mesh refinement increases from 1 element to 8 elements. The interface file is then used to control the position of the bottom of the new cube as if it underwent the same impact as the cube in run one..

Model:

The material of the cube and the plate are elastic. The plate, that measures $40 \times 40 \times 2$ mm³, is modeled with 16 Belytschko-Tsay shell elements. The cube has a side length of 10 mm and is initially positioned 10 mm above the plate. The cube is given an initial velocity towards the plate.

Reference:

Schweizerhof, K. and Weimer, K.

***INTERFACE_COMPONENT**
An Interface File Controls the Response of a Cube

```

$      hgen      rwen      slnten      rylen
$          2
$
$ *CONTROL_HOURLASS
$      ihq      qh
$          4
$
$$$$ opifs - output interval for interface file
$
$ *CONTROL_OUTPUT
$      npopt      neecho      nrefup      iaccop      opifs      ipnint      ikedit
$                                0.002E-3
$
$ *CONTROL_TIMESTEP
$      dtinit      scft      isdo      tslimt      dtms      lctm      erode      mslst
$                                0.10
$
$ *DATABASE_BINARY_D3PLOT
$      dt      lcdt
$      0.00002
$
$ *DATABASE_BINARY_D3THDT
$      dt      lcdt
$      0.00001
$
$ *DATABASE_EXTENT_BINARY
$      neiph      neips      maxint      strflg      sigflg      epsflg      rtlflg      engflg
$                                1
$      cmpflg      ieverp      beamip
$
$
$ *DATABASE_GLSTAT
$
$      dt
$      0.00001
$
$ *DATABASE_NODOUT
$      dt
$      0.00001
$
$ *DATABASE_HISTORY_NODE
$      id1      id2      id3      id4      id5      id6      id7      id8
$      101      201      205
$
$ *DATABASE_RCFORC
$      dt
$      0.00001
$
$$$$ Interface
$
$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
$$$$ Link the interface file to the following segments.
$
$ *INTERFACE_LINKING_SEGMENT
$      ssid      ifid
$          3      1
$
$ *SET_SEGMENT

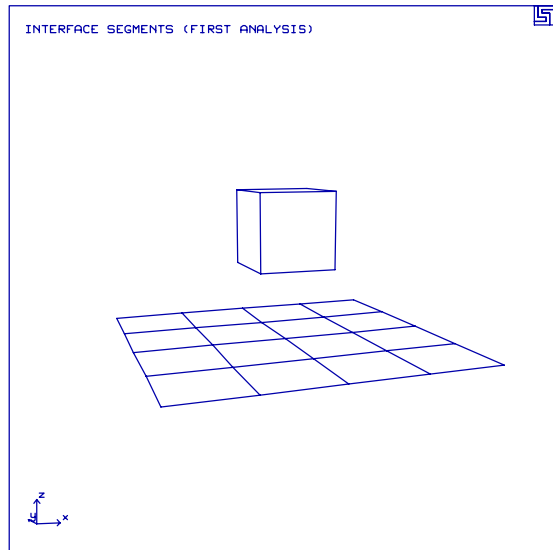
```


*INTERFACE_COMPONENT

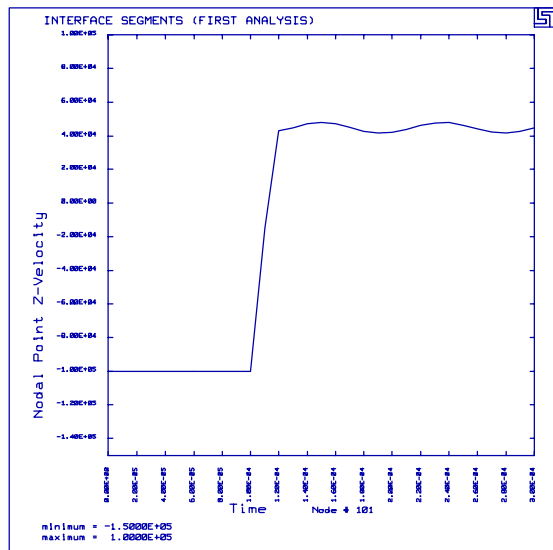
An Interface File Controls the Response of a Cube

Results:

taurus g=d3plot
19
rz 20 rx -80 center v



phs3
nodout
oaset -1.5e5 1.0e5 z-vel 101

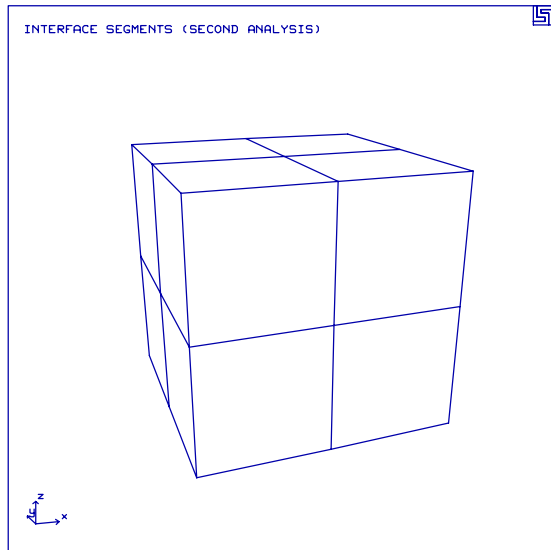


*INTERFACE_COMPONENT

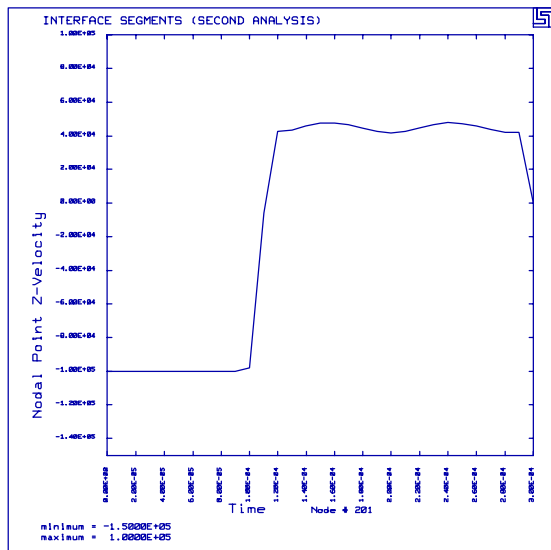
An Interface File Controls the Response of a Cube

Results:

taurus g=d3plot
19
rz 20 rx -70 center v



phs3
nodout
oset -1.5e5 1.0e5 z-vel 201



***INTERFACE_COMPONENT**

An Interface File Controls the Response of a Cube

LS-DYNA Manual Section: *LOAD_BODY_GENERALIZED

Additional Sections:

*BOUNDARY_PRESCRIBED_MOTION_NODE
*DATABASE_CROSS_SECTION_SET
*INITIAL_VELOCITY_NODE

Example: Rotating Elements

Filename: load_body.shell.k

Description:

A body has constant angular velocity. The radial vibration introduced due to the rapid deployment of the rotation is damped out in the initialization phase using dynamic relaxation.

Model:

The body measures $200 \times 100 \times 10 \text{ mm}^3$. The body consists of 2 Belytschko-Tsay elastic shell elements. The body rotates about the y-axis at 62.83 radians per second. The analysis ends at 0.1 seconds.

Input:

All nodes have an initial translational velocity based on the angular velocity $v = \omega \times r$. (*INITIAL_VELOCITY_NODE). Dynamic relaxation damps oscillations in the radial direction during the initialization (*LOAD_BODY_GENERALIZED, *DEFINE_CURVE). This essentially pre-stresses the structure and the load continues into the analysis portion. Because of the condition of constant angular velocity of the two nodes on the axis of rotation, the motion remains uniform throughout the calculation (*BOUNDARY_PRESCRIBED_MOTION_NODE). The section forces are available in the ASCII database file secforc (*DATABASE_SECFORC).

Reference:

Schweizerhof, K. and Weimer, K.

*LOAD_BODY_GENERALIZED

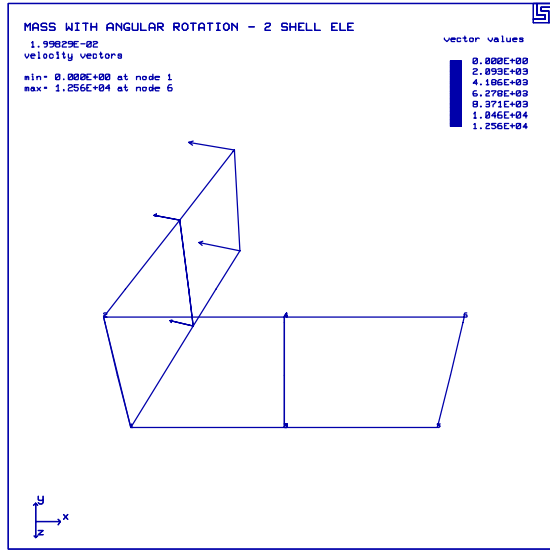
Rotating Elements

```
$      n1      n2      lcid  drlcid      xc      yc      zc
      1      6      0      2      0.0    0.0    0.0
$      ax      ay      az      omx      omy      omz
      0.0    0.0    0.0    0.0    1.0    0.0
$
*DEFINE_CURVE
$      lcid      sidr      scla      sclo      offa      offo
      2      1
$      abscissa      ordinate
      0.000      62.83
      1.000      62.83
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*PART
$      pid      sid      mid      eosid      hgid      adpopt
shells
      1      1      1
$
$
*MAT_ELASTIC
$      mid      ro      e      pr      da      db      k
      1 1.00e-08 210000. 0.300
$
$
*SECTION_SHELL
$      sid      elform      shrf      nip      propt      qr/irid      icomp
      1      3
$      t1      t2      t3      t4      nloc
      10.0    10.0    10.0    10.0
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Nodes and Elements
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
*NODE
$      node      x      y      z      tc      rc
      1 0.000000E+00 0.000000E+00 0.000000E+00 7 0
      2 0.000000E+00 1.000000E+02 0.000000E+00 6 0
      3 1.000000E+02 0.000000E+00 0.000000E+00 0 0
      4 1.000000E+02 1.000000E+02 0.000000E+00 0 0
      5 2.000000E+02 0.000000E+00 0.000000E+00 0 0
      6 2.000000E+02 1.000000E+02 0.000000E+00 0 0
$
*ELEMENT_SHELL
$      eid      pid      n1      n2      n3      n4
      1      1      1      3      4      2
      2      1      3      5      6      4
$
*END
```

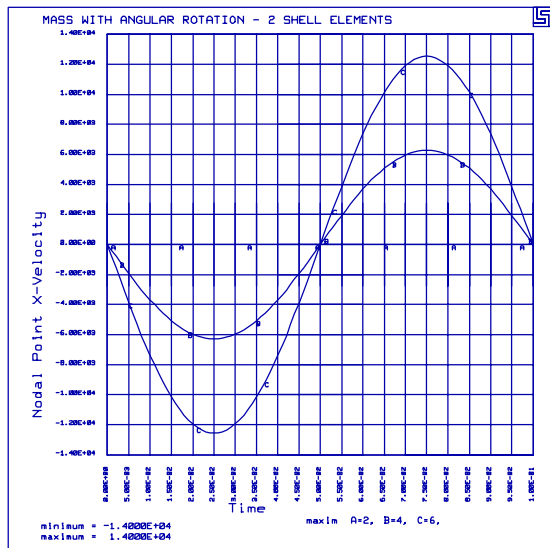
*LOAD_BODY_GENERALIZED Rotating Elements

Results:

taurus g=d3plot
19
ytran -80 rx 40 ndplt s 3 over vect velo



phs3
nodout
grid oset -1.4e4 1.4e4 x-vel 2 4 6



***LOAD_BODY_GENERALIZED**

Rotating Elements

LS-DYNA Manual Section: *LOAD_BODY_Z

Additional Sections:

*RIGIDWALL_PLANAR

Example: Tire Under Gravity Loading Bounces on a Rigid Wall

Filename: load_body.gravity.k

Description:

A simple model of a tire is placed under gravity loaded and bounces on a rigid wall.

Model:

A positive gravity constant of 0.00981 mm/ms^2 is used to make the tire drop in the negative z-direction. A *RIGIDWALL_PLANAR keyword is used to define the ground. Nodes on the bottom of the tire are prevented from penetrating the rigid wall by specifying them within the *RIGIDWALL_PLANAR command (using a *SET_NODE_COLUMN keyword).

Results:

The rigid wall forces oscillate about the steady state, which is the weight of the tire ($W = 0.26 \text{ kN}$). Curiously, the tire damps out even though no damping is specified within the model. See the example in *DAMPING_GLOBAL for an explanation and fix.

***LOAD_BODY_Z**

Tire Under Gravity Loading Bounces on a Rigid Wall

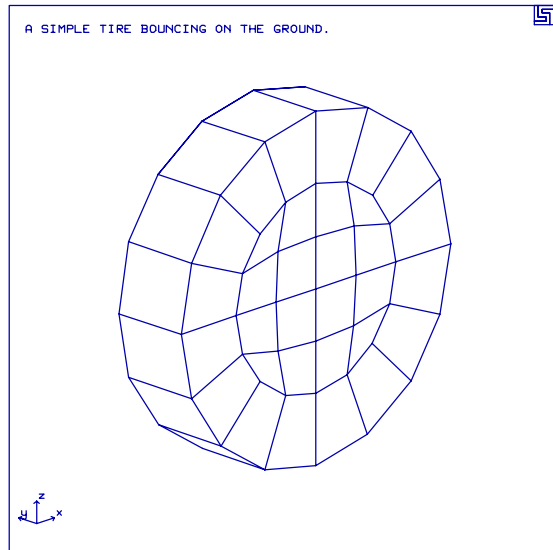
```
.
8931 2.790000000E+02 -7.54000000E+02 0.000000000E+00 0 0
8932 2.577620000E+02 -7.54000000E+02 1.067690000E+02 0 0
$
$$$$$$$ Shell Elements
$
*ELEMENT_SHELL
$  eid      pid      n1      n2      n3      n4
  8710      35      8719      8722      8723      8720
  8711      35      8720      8723      8724      8721
.
... in total, 96 shells defined
.
8948      36      8928      8931      8932      8929
8949      36      8929      8932      8926      8924
$
$$$$$$$ Nodal Mass Elements
$
*ELEMENT_MASS
$  eid      nid      mass
  8730      8730      10.0
  8746      8746      10.0
$
*END
```

*LOAD_BODY_Z

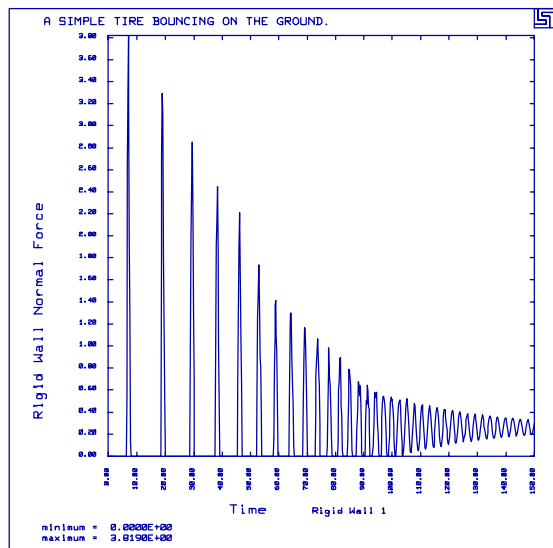
Tire Under Gravity Loading Bounces on a Rigid Wall

Results:

taurus g=d3plot
angle 1 rx -90
ry 45 rx 20 view



phs3
rwforc
normal



***MAT_FRAZER_NASH_RUBBER_MODEL**
Frazer-Nash Single Element

LS-DYNA Manual Section: *MAT_FRAZER_NASH_RUBBER_MODEL

Example: Frazer-Nash Single Element

Filename: mat_fn_rubber.element.k

Description:

This model illustrates the behavior of the Frazer Nash rubber model using a single element.

Model:

The example contains a single element which measures $7.5 \times 7.5 \times 100$. The element is constrained in the z-direction on the bottom and has prescribed velocity on the top surface.

Input:

Unitary input for any constant indicates least squares curve fitting. (*MAT_FRAZER_NASH_RUBBER). The least squares curve fit requires specimen dimensions and a stress-strain load curve. The model provides the option to stop the calculation based on maximum and minimum strain values.

Results:

The compressibility of the element and the pressure versus average strain are shown in the plots..

References:

Kennington, D. C.

***MAT_FRAZER_NASH_RUBBER_MODEL**
Frazer-Nash Single Element

```

$     dt
     0.1
$
*DATABASE_HISTORY_NODE
$   id1      id2      id3      id4      id5      id6      id7      id8
     1
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Boundary Conditions - Prescribed Motion
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*BOUNDARY_PRESCRIBED_MOTION_NODES
$   nid      dof      vad      lcid      sf      vid
     1         4         2         1 4.000E-02     1
     2         4         2         1 4.000E-02     1
     3         4         2         1 4.000E-02     1
     4         4         2         1 4.000E-02     1
$
*DEFINE_VECTOR
$   vid      xt      yt      zt      xh      yh      zh
     1 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00-1.000E+00
$
*DEFINE_CURVE
$   lcid      sidr      scla      sclo      offa      offo
     1
$   abscissa      ordinate
     0.00000000E+00      0.00000000E+00
     2.00000000E+00      7.13000011E+00
     4.00000000E+00      1.35200005E+01
     6.00000000E+00      1.86100006E+01
     8.00000000E+00      2.18700008E+01
     1.00000000E+01      2.30000000E+01
     1.20000000E+01      2.18700008E+01
     1.40000000E+01      1.86100006E+01
     1.60000000E+01      1.35200005E+01
     1.80000000E+01      7.13000011E+00
     2.00000000E+01      0.00000000E+00
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*PART
$   pid      sid      mid      eosid      hgid      adpopt
Rubber
     1         1         1
$
$
*MAT_FRAZER_NASH_RUBBER_MODEL
$   mid      ro      pr      c100      c200      c300      c400
     1 1.254E-06      0.495 1.000E+00 0.000E+00
$
$   c110      c210      c010      c020      exit      emax      emin
     1.000E+00 0.000E+00 1.000E+00 1.000E+00 1.000E+00 9.000E-01-9.000E-01

```

***MAT_FRAZER_NASH RUBBER_MODEL**

Frazer-Nash Single Element

```

$
$       sgl       sw       st       lcid
   1.000E+00 1.000E+00 1.000E+00         2
$
$
*SECTION_SOLID
$       sid       elform
       1         0
$
$$$$ Force versus actual change in guage length for F_N rubber model.
$
*DEFINE_CURVE
$       lcid       sidr       scla       sclo       offa       offo
       2
$
$       abscissa           ordinate
0.00000000E+00   0.00000000E+00
6.07299991E-03   3.59800004E-04
1.24500003E-02   6.25399989E-04
1.88100003E-02   8.85999994E-04
2.53199991E-02   1.24600006E-03
3.11200004E-02   1.71500002E-03
3.71199995E-02   2.40099989E-03
4.32099998E-02   3.35399993E-03
4.92900014E-02   4.59800009E-03
5.42900003E-02   5.86300017E-03
5.93000017E-02   7.36099994E-03
6.43299967E-02   9.10999998E-03
6.94399998E-02   1.11400001E-02
7.27799982E-02   1.26200002E-02
7.60900006E-02   1.41899996E-02
7.94499964E-02   1.59000009E-02
8.28600004E-02   1.77500006E-02
8.40499997E-02   1.84300002E-02
8.52300003E-02   1.91099998E-02
8.64199996E-02   1.98199991E-02
8.76099989E-02   2.05400009E-02
1.08700001E+00   2.01999998E+00
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Nodes and Elements
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
*NODE
$       node       x           y           z           tc           rc
       1 7.50000000E+00 0.00000000E+00 1.00000000E+01 0 0
       2 7.50000000E+00 7.50000000E+00 1.00000000E+01 0 0
       3 0.00000000E+00 7.50000000E+00 1.00000000E+01 0 0
       4 0.00000000E+00 0.00000000E+00 1.00000000E+01 0 0
       5 7.50000000E+00 0.00000000E+00 0.00000000E+00 3 0
       6 7.50000000E+00 7.50000000E+00 0.00000000E+00 3 0
       7 0.00000000E+00 7.50000000E+00 0.00000000E+00 3 0
       8 0.00000000E+00 0.00000000E+00 0.00000000E+00 3 0
$
*ELEMENT_SOLID
$       eid       pid       n1       n2       n3       n4       n5       n6       n7       n8
       1         1         5         6         7         8         1         2         3         4
$
*END

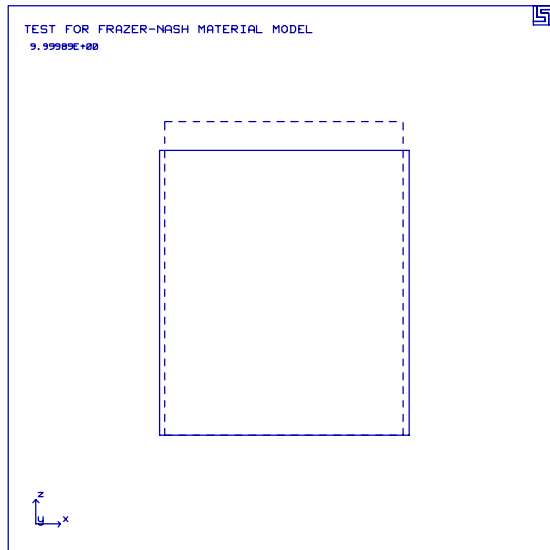
```

*MAT_FRAZER_NASH_RUBBER_MODEL

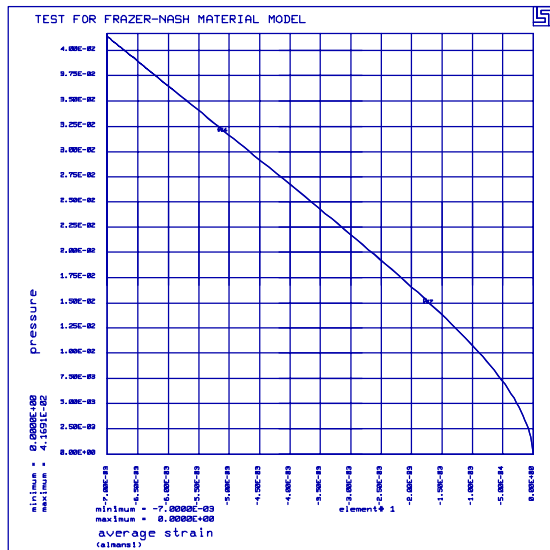
Frazer-Nash Single Element

Results:

taurus g=d3plot
 19
 rx -90 angle 1 dist 1000 udg 1 state 101 view



phs2
 element 1 1 gather
 grid aset -7e-3 0 e2hist 8 308 1 1



***MAT_FRAZER_NASH_RUBBER_MODEL**

Frazer-Nash Single Element

***MAT_PIECEWISE_LINEAR_PLASTICITY** Piecewise Linear Plasticity Fragmenting Plate

LS-DYNA Manual Section: *MAT_PIECEWISE_LINEAR_PLASTICITY

Example: Piecewise Linear Plasticity Fragmenting Plate

Filename: mat_piecewise_linear.plate-shatter.k

Description:

A plate of 1,200 Belytschko-Tsay shell elements strikes a wall at an angle of 45 degrees from the wall normal. The impact velocity is 20,775 in/sec. and the termination time is 0.00025 seconds.

Model:

The material description contains Young's Modulus, Poisson's ratio, yield stress, hardening modulus, ultimate plastic strain, and time step size for element deletion.

Input:

One material definition for a Belytschko-Tsay shell with viscous hourglass control (*CONTROL_HOURLASS). Young's Modulus, Poisson's ratio, yield stress and the hardening modulus are 16 Msi, 0.35, 155,000 psi, and 192,000 psi respectively. (*MAT_LINEAR_PIECEWISE_PLASTICITY). The plastic strain at failure is 32% and the failure minimum time step size is 0.3 μ seconds.

Results:

The plate deforms away from the stonewall and the plate fragments.

*MAT_PIECEWISE_LINEAR_PLASTICITY

Piecewise Linear Plasticity Fragmenting Plate

List of LS-DYNA input deck:

```
*KEYWORD
*TITLE
Test for Material 24 with Failure
$
$ LSTC Example
$
$ Last Modified: September 18, 1997
$
$ Units: lbf-s2/in, in, s, lbf, psi, lbf-in
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*CONTROL_TERMINATION
$ endtim endcyc dtmin endneg endmas
 2.500E-04 5.000E-02
$
*CONTROL_CONTACT
$ slsfac rwpnal islchk shlthk penopt thkchg orien
 0.01
$ usrstr usrfac nsbcs interm xpenen
$
$
*CONTROL_HOURLGLASS
$ ihq qh
 4
$
*DATABASE_BINARY_D3PLOT
$ dt/cycl lcdt
 1.250E-05
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Initial Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
$$$$ All nodes except nodes in node set 1 are given an initial velocity.
$$$$ Node set 1 contains the nodes of the wall.
$
*INITIAL_VELOCITY
$ nsid nsidex boxid
 1
$
$ vx vy vz vxr vyr vzr
-1.469E+04 -1.469E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00
$
$ vxe vye vze vxre vyre vzre
$
$
*SET_NODE_LIST
$ sid
 1
$ nid1 nid2 nid3 nid4 nid5 nid6 nid7 nid8
 1282 1283 1284 1285
```


*MAT_PIECEWISE_LINEAR_PLASTICITY

Piecewise Linear Plasticity Fragmenting Plate

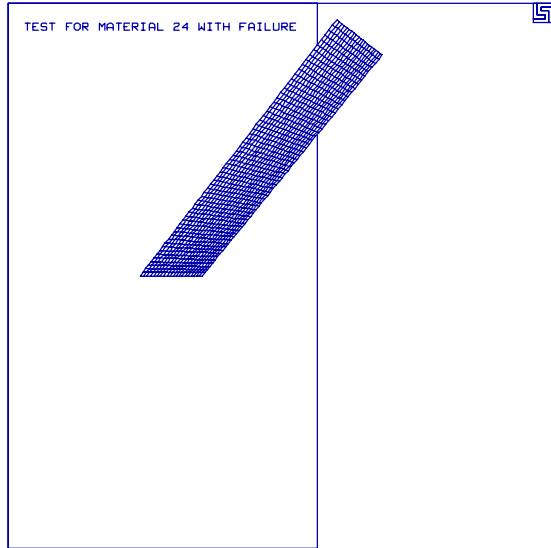
```
*NODE
$  node          x          y          z          tc          rc
   1  0.000000E+00  0.000000E+00  0.000000E+00    0          0
   .
   ... in total, 1285 nodes defined
   .
  1285 -5.000000E-02 -1.000000E+01  5.000000E+00    7          7
$
$$$$$ Shell Elements
$
*ELEMENT_SHELL
$  eid          pid          n1          n2          n3          n4
   1           2           22           1           2           23
   .
   ... in total, 1201 shells defined
   .
  1201          3          1282          1283          1284          1285
$
*END
```

*MAT_PIECEWISE_LINEAR_PLASTICITY

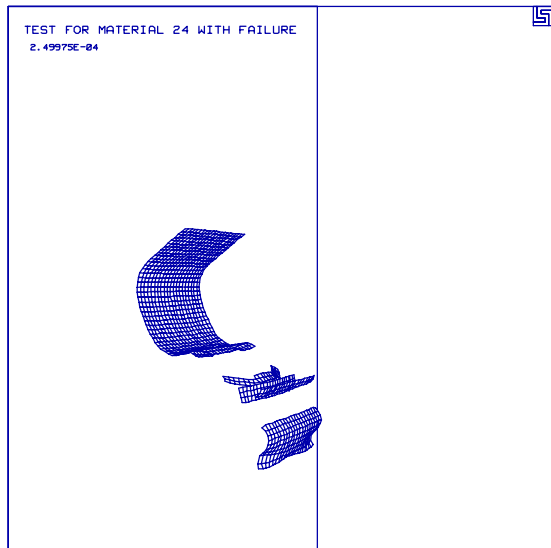
Piecewise Linear Plasticity Fragmenting Plate

Results:

taurus g=d3plot
19
ry -30 dist 12 view



state 21
view



***MAT_PIECEWISE_LINEAR_PLASTICITY**
Piecewise Linear Plasticity Fragmenting Plate

LS-DYNA Manual Section: *MAT_RIGID**Additional Sections:**

*DEFINE_COORDINATE_VECTOR
*LOAD_SEGMENT

Example: Rigid Sliding Block in Local Coordinate System

Filename: mat_rigid.block-slide.k

Description:

A center of mass is constrained to slide along a local coordinate system. The termination time is 0.010 seconds.

Model:

The material description references a local coordinate system to constrain the rigid block. The rigid block is free to translate along the local z axis.

Input:

The material definition is a rigid material (*MAT_RIGID). The material specifies the use of a local coordinate system, the local coordinate constraint value of 100111 (tx ty tz rx ry rz), and the local coordinate system for output. The local coordinate system specifies that the local origin is the global origin, the local x-axis point is (1.0,0.0,1.0) and the local y-axis point is (0.0,0.0,1.0) (*DEFINE_COORDINATE_VECTOR).

A shell element is defined in order to control the timestep.

Results:

The block slides along the local coordinate system.

*MAT_RIGID

Rigid Sliding Block in Local Coordinate System

List of LS-DYNA input deck:

```

*KEYWORD
*TITLE
Sliding Block
$
$  LSTC Example
$
$  Last Modified: September 18, 1997
$
$  Units: lbf-s2/in, in, s, lbf, psi, lbf-in
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Control Output
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONTROL_TERMINATION
$  endtim  endcyc  dtmin  endneg  endmas
  1.000E-02
$
*DATABASE_BINARY_D3PLOT
$  dt  lcdt
  5.000E-04
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*PART
$  pid  sid  mid  eosid  hgid  adpopt
block  1  1  1
plate  2  2  2
$
$
*MAT_RIGID
$  mid  ro  e  pr  n  couple  m  alias
  1  7.85e-04  30.00e+06  0.300
$
$  cmo  con1  con2
  -1.0  1.0  100111
$
$  lco/a1  a2  a3  v1  v2  v3
  1.0
$
*DEFINE_COORDINATE_VECTOR
$  cid  xt  yt  zt  xh  yh  zh
  1  1.000E+00  0.000E+00  1.000E+00  0.000E+00  0.000E+00  1.000E+00
$
*MAT_ELASTIC
$  mid  ro  e  pr  da  db  k
  2  7.85e-04  30.00e+06  0.300
$

```

***MAT_RIGID**
Rigid Sliding Block in Local Coordinate System

```

$
*SECTION_SOLID
$    sid    elform
$      1      0
$
$
*SECTION_SHELL
$    sid    elform      shrf      nip      propt    qr/irid      icomp
$      2
$    t1      t2      t3      t4      nloc
$    1.0      1.0      1.0      1.0
$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Loading
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
$
*LOAD_SEGMENT
$    lcid      sf      at      n1      n2      n3      n4
$      1 1.000E+00 0.000E+00      53      49      50      54
$      1 1.000E+00 0.000E+00      57      53      54      58
$      1 1.000E+00 0.000E+00      61      57      58      62
$      1 1.000E+00 0.000E+00      54      50      51      55
$      1 1.000E+00 0.000E+00      58      54      55      59
$      1 1.000E+00 0.000E+00      62      58      59      63
$      1 1.000E+00 0.000E+00      55      51      52      56
$      1 1.000E+00 0.000E+00      59      55      56      60
$      1 1.000E+00 0.000E+00      63      59      60      64
$
$
*DEFINE_CURVE
$    lcid      sidr      scla      sclo      offa      offo
$      1
$      abscissa      ordinate
$      0.000E+00      1.000E+02
$      1.000E-02      1.000E+02
$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Nodes and Elements
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
$
*NODE
$    node      x      y      z      tc      rc
$      1      0.000000E+00      0.000000E+00      0.000000E+00      0      0
$      2      3.333333E-01      0.000000E+00      0.000000E+00      0      0
$      3      6.666667E-01      0.000000E+00      0.000000E+00      0      0
$      .
$      ... in total, 68 nodes defined
$      .
$      66      1.000000E+00      0.000000E+00      -1.000000E+00      0      0
$      67      0.000000E+00      1.000000E+00      -1.000000E+00      0      0
$      68      1.000000E+00      1.000000E+00      -1.000000E+00      0      0
$
$
$$$$$ Solid Elements
$
*ELEMENT_SOLID
$    eid      pid      n1      n2      n3      n4      n5      n6      n7      n8

```

*MAT_RIGID

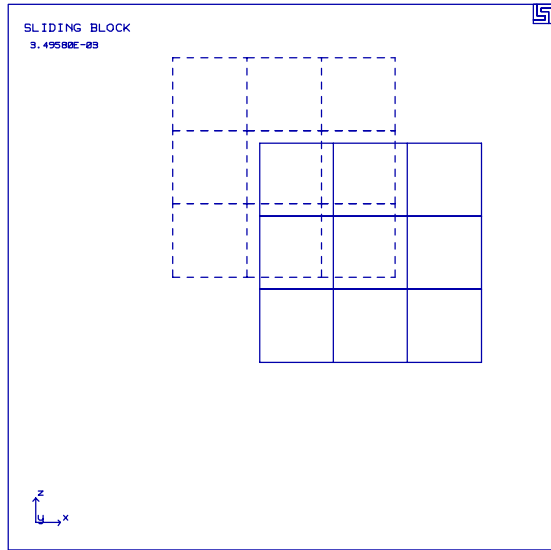
Rigid Sliding Block in Local Coordinate System

```
1      1      1      2      6      5      17      18      22      21
2      1      2      3      7      6      18      19      23      22
3      1      3      4      8      7      19      20      24      23
.
... in total, 27 solids defined
.
25     1     41     42     46     45     57     58     62     61
26     1     42     43     47     46     58     59     63     62
27     1     43     44     48     47     59     60     64     63
$
$$$$$ Shell Element - used to control the timestep
$
*ELEMENT_SHELL
$   eid   pid   n1   n2   n3   n4
    1     2    65   67   68   66
*END
```

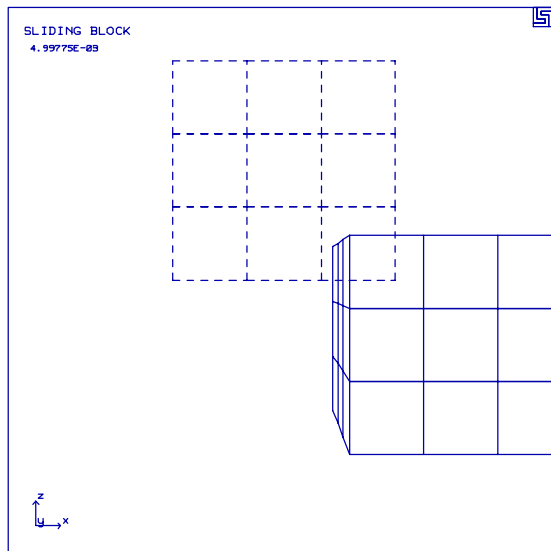
Rigid Sliding Block in Local Coordinate System

Results:

taurus g=d3plot
19
m 1 udg 1 rx -90 state 8 view



state 11
view



***MAT_RIGID**

Rigid Sliding Block in Local Coordinate System

LS-DYNA Manual Section: *MAT_SOIL_AND_FOAM

Example: Soil and Foam Single Element

Filename: mat_soil_foam.element.k

Description:

This problem contains a single element with one degree of freedom on a side. The element compresses and expands.

Model:

The element measures 100 cubic inches. One side follows a velocity curve which results in a range of relative volume (V/V_0) 1.000 to 0.0091 to 1.441.

Input:

The foam follows a pressure volumetric strain relationship (*MAT_SOIL_AND_FOAM). The unloading behavior may follow either the unloading bulk modulus or the loading curve. The unloading in the first case follows the bulk modulus, while the unloading in the second case follows the loading curve. The material has a cutoff pressure of 0.5.

Results:

The plots show the element pressure versus time.

*MAT_SOIL_AND_FOAM

Soil and Foam Single Element

```
$  
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$  
$...>....1...>....2...>....3...>....4...>....5...>....6...>....7...>....8  
$  
*BOUNDARY_PRESCRIBED_MOTION_SET  
$      nid      dof      vad      lcid      sf      vid  
      1         3         0         1         1.0       0  
$  
*DEFINE_CURVE  
$      lcid      sidr      scla      sclo      offa      offo  
      1  
$      abscissa      ordinate  
      0.000E+00      -9.000E+02  
      1.000E-01      -9.000E+02  
      1.010E-01      9.000E+02  
      2.500E-01      9.000E+02  
$  
*SET_NODE_LIST  
$      sid  
      1  
$      nid1      nid2      nid3      nid4      nid5      nid6      nid7      nid8  
      5         6         7         8  
$  
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$  
$  
$$$$ Define Parts and Materials  
$  
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$  
$...>....1...>....2...>....3...>....4...>....5...>....6...>....7...>....8  
$  
*PART  
$      pid      sid      mid      eosid      hgid      adpopt  
foam block  
      1         1         1  
$  
*MAT_SOIL_AND_FOAM  
$      mid      ro      bulk      g      a0      a1      a2      pc  
      1 6.740E-11 5.760E+01 1.794E+01 1.200E-01 0.000E+00 0.000E+00 -5.000E-01  
$      f      f  
$      vcr      dun  
$  
$ Unloading follows the loading curve  
$ 1.000E+00 0.000E+00  
$  
$ Bulk unloading modulus is used - volumetric crushing  
  0.000E+00 0.000E+00  
$  
$      eps1      eps2      eps3      eps4      eps5      eps6      eps7      eps8  
-2.500E-02 -5.000E-02 -1.050E-01 -3.570E-01 -6.930E-01 -9.160E-01 -1.200E+00 -1.610E+00  
$  
$      eps9      eps10  
  0.000E+00 0.000E+00  
$  
$      p1      p2      p3      p4      p5      p6      p7      p8  
 3.450E-01 5.170E-01 6.890E-01 8.070E-01 1.110E+00 1.240E+00 1.300E+00 1.500E+00  
$  
$      p9      p10  
  0.000E+00 0.000E+00  
$  
*SECTION_SOLID  
$      sid      elform  
      1
```

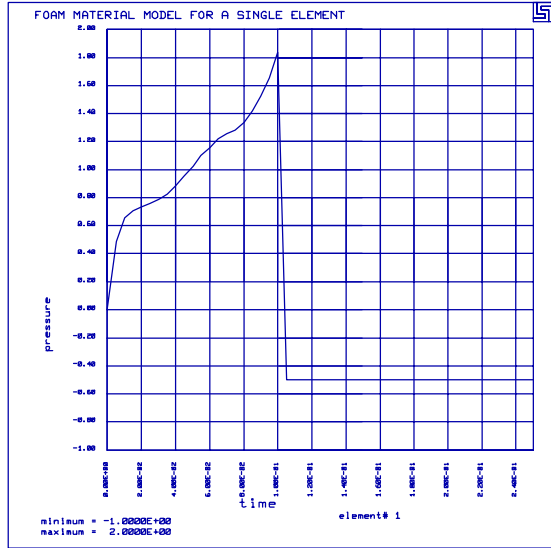

Results:

Volumetric Crushing

taurus g=d3plot

19

phs2 elem 1 1 gather grid oset -1 2 etime 8 1 1

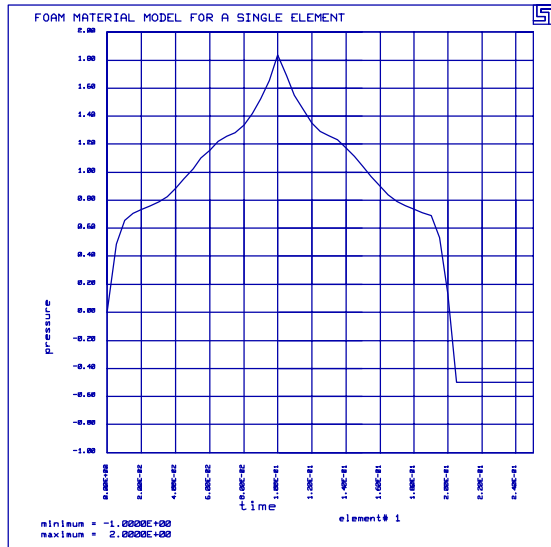


Unloading Follows Loading Curve

taurus g=d3plot

phs2

elem 1 1 gather grid oset -1 2 etime 8 1 1



***MAT_SOIL_AND_FOAM**
Soil and Foam Single Element

LS-DYNA Manual Section: *MAT_SPRING

Additional Sections:

- *CONSTRAINED_EXTRA_NODES_SET
- *CONSTRAINED_JOINT_SPHERICAL
- *CONTACT_SURFACE_TO_SURFACE
- *DEFINE_SD_ORIENTATION
- *ELEMENT_DISCRETE
- *LOAD_BODY_Z
- *MAT_DAMPER_VISCOUS
- *PART_INERTIA

Example: Belted Dummy with Springs

Filename: mat_spring.belted-dummy.k

Description:

This is a simulation of the interaction between a dummy and seating system. The dummy has an initial velocity, base vehicle acceleration, and decelerated base.

Model:

The dummy consists of 15 ellipsoidal rigid bodies connected through cylindrical joints, springs and dampers. The base of the seat belts and the seat decelerates backwards relative to the dummy.

Input:

The dummy consists of rigid bodies 1 through 15. Materials 16 through 20 define the seat and material 21 and 22 define the seat belt. The rigid bodies are constrained with respect to each other with spherical joints (*CONSTRAINED_JOINT_SPHERICAL). Discrete springs and dampers between the rigid body provide the relative stiffness and viscosity. The initial velocity of all nodes is 14.8 units, while the acceleration of the seat and belt ends follow an acceleration curve in the opposite direction.

Results:

LS-DYNA predicts that the dummy slides under the seat belts.

Reference:

Stillman, D. W.

*MAT_SPRING

Belted Dummy with Springs

List of LS-DYNA input deck:

```

*KEYWORD
*TITLE
Belted Dummy
$
$ LSTC Example
$
$ Last Modified: September 19, 1997
$
$ Units: kg, m, s, N, Pa, Joule
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Control Output
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONTROL_TERMINATION
$ endtim endcyc dtmin endneg endmas
1.200E-01
$
*CONTROL_CONTACT
$ slsfac rwpnal islchk shlthk penopt thkchg orien
2
$ usrstr usrfac nsbcs interm xpenen
$
*CONTROL_TIMESTEP
$ dtinit scft isdo tslimt dtms lctm erode mslst
0.000E+00 8.000E-01 0 0.000E+00 0.000E+00 0 0
$
$
*DATABASE_BINARY_D3PLOT
$ dt/cycl lcdt
2.500E-03
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Initial Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
$$$$ All nodes are given an initial velocity.
$
*INITIAL_VELOCITY
$ nsid nsidex boxid
0
$
$ vx vy vz vxr vyr vzr
1.480E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Boundary Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$

```


***MAT_SPRING**
Belted Dummy with Springs

```

$      lcid      sf      lciddr
      51      1.00      0

$
*DEFINE_CURVE
$      lcid      sidr      scla      sclo      offa      offo
      51
$      abscissa      ordinate
      0.00000000E+00      9.81
      1.51999995E-01      9.81

$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Contacts - Sliding Interfaces
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
$$$$$ The segment sets associated with these contacts are located at the end
$$$$$ of this file.
$
*CONTACT_SURFACE_TO_SURFACE
$      ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
      1      2      0      0      vdc      penchk      bt      dt
      6.200E-01
$      sfs      sfm      sst      mst      sfst      sfmt      fsf      vsf

$
*CONTACT_SURFACE_TO_SURFACE
$      ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
      3      4      0      0      vdc      penchk      bt      dt
      6.200E-01
$      sfs      sfm      sst      mst      sfst      sfmt      fsf      vsf

$
*CONTACT_SURFACE_TO_SURFACE
      5      6      0      0
      6.200E-01

$
*CONTACT_SURFACE_TO_SURFACE
      7      8      0      0
      8.000E-01

$
*CONTACT_SURFACE_TO_SURFACE
      9      10      0      0
      1.000E+00

$
*CONTACT_SURFACE_TO_SURFACE
      11      12      0      0
      8.000E-01

$
*CONTACT_SURFACE_TO_SURFACE
      13      14      0      0
      8.800E-01

$

```

*MAT_SPRING Belted Dummy with Springs

```

*CONTACT_SURFACE_TO_SURFACE
  15    16    0    0
  8.800E-01

$
*CONTACT_SURFACE_TO_SURFACE
  17    18    0    0
  1.600E-01

$
*CONTACT_SURFACE_TO_SURFACE
  19    20    0    0
  8.800E-01

$
*CONTACT_SURFACE_TO_SURFACE
  21    22    0    0
  0.000E+00

$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Constraints
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONSTRAINED_JOINT_SPHERICAL
$      n1      n2      n3      n4      n5      rps      damp
      99      227      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
      228      405      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
      406      865      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
      866      971      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
      407      537      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
      538      685      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
      408      603      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
      604      763      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
      972      1097     0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
      1098     1497     0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
      1498     1645     0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
      973      1317     0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
      1318     1579     0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
      1580     1733     0      0      0      0 0.000E+00

$
$
*CONSTRAINED_EXTRA_NODES_SET
$      pid      nsid
      1         2
  
```

***MAT_SPRING**
Belted Dummy with Springs

```

$
*SET_NODE_LIST
$   sid
    2
$   nid1      nid2      nid3      nid4      nid5
    99       100       101       102
$
.
... in total, 15 extra_nodes_set & set_node_list pairs defined
.
$
*CONSTRAINED_EXTRA_NODES_SET
$   pid      nsid
    2        3
$
*SET_NODE_LIST
$   sid
    3
$   nid1      nid2      nid3      nid4      nid5      nid6      nid7      nid8
    227       228       229       230       231       232       233       234
$
$
$$$$ Define Spring Orientation Vectors and Curves
$
$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*DEFINE_SD_ORIENTATION
$   vid      iop      xt      yt      zt      nid1      nid2
    1        2 0.000E+00 0.000E+00 0.000E+00      100      229
    2        2 0.000E+00 0.000E+00 0.000E+00      101      230
    3        2 0.000E+00 0.000E+00 0.000E+00      102      231
.
... in total, 42 sd_orientation vectors defined
.
    40       2 0.000E+00 0.000E+00 0.000E+00      1584     1734
    41       2 0.000E+00 0.000E+00 0.000E+00      1585     1735
    42       2 0.000E+00 0.000E+00 0.000E+00      1586     1736
$
$$$$ Define Curves
$
*DEFINE_CURVE
$   lcid      sidr      scla      sclo      offa      offo
    1
$   abscissa      ordinate
-1.71000004E+00    -5.38000000E+02
-7.09999979E-01    -8.47500000E+01
-6.80000007E-01    -7.76600037E+01
-6.60000026E-01    -7.10599976E+01
-5.89999974E-01    -5.36800003E+01
-5.00000000E-01    -4.05800018E+01
-3.89999986E-01    -2.99799995E+01
-2.09999997E-02    -4.65000010E+00
0.00000000E+00     0.00000000E+00
2.09999997E-02     4.65000010E+00
3.89999986E-01     2.99799995E+01
5.00000000E-01     4.05800018E+01
5.89999974E-01     5.36800003E+01

```


*MAT_SPRING

Belted Dummy with Springs

```

part-22
  22      22      22      0
spring 101
  101     101     101
$
.
... spring pid's 102-207 also defined here
.
$
spring 208
  208     208     208
$
$$$$$$$ Materials
$
$
$$$$ Rigid Materials
$
*MAT_RIGID
$   mid      ro      e      pr      n      couple      m      alias
    1 4.064E+03 4.000E+08 3.000E-01 0.000E+00 0.000E+00 0.000E+00
    0.000E+00 0.000E+00 0.000E+00
    0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
$
.
... mat_rigid mid's 2-14 also defined here
.
$
*MAT_RIGID
$   mid      ro      e      pr      n      couple      m      alias
    15 2.000E+03 4.000E+08 3.000E-01 0.000E+00 0.000E+00 0.000E+00
    0.000E+00 0.000E+00 0.000E+00
    0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
$
$
$$$$ Elastic Materials
$
*MAT_ELASTIC
$   mid      ro      e      pr      da      db      k
    16 4.646E+03 4.000E+08 3.000E-01
*MAT_ELASTIC
$   mid      ro      e      pr      da      db      k
    17 4.646E+03 4.000E+08 3.000E-01
*MAT_ELASTIC
$   mid      ro      e      pr      da      db      k
    18 4.646E+03 4.000E+09 3.000E-01
*MAT_ELASTIC
$   mid      ro      e      pr      da      db      k
    19 4.646E+03 4.000E+08 3.000E-01

*MAT_ELASTIC
$   mid      ro      e      pr      da      db      k
    20 2.000E+03 4.100E+08 3.000E-01
*MAT_ELASTIC
$   mid      ro      e      pr      da      db      k
    21 2.000E+03 4.100E+08 3.000E-01
*MAT_ELASTIC
$   mid      ro      e      pr      da      db      k
    22 4.000E+03 2.000E+08 3.000E-01
$
$
$$$$ Nonlinear Elastic Spring Materials
$
*MAT_SPRING_NONLINEAR_ELASTIC

```

***MAT_SPRING**
Belted Dummy with Springs

```

101      1
$
.
... mat_spring_nonlinear_elastic mid's 101-142 also defined here
.
$
*MAT_SPRING_NONLINEAR_ELASTIC
142      42
$
$
$$$$ Viscous Damper Materials
$
*MAT_DAMPER_VISCOUS
143 2.300E+00
$
.
... mat_damper_viscous mid's 143-184 also defined here
.
$
*MAT_DAMPER_VISCOUS
184 1.000E+00
$
$
$$$$ Nonlinear Viscous Damper Materials
$
*MAT_DAMPER_NONLINEAR_VISCOUS
185      43
$
.
... mat_damper_nonlinear_viscous mid's 185-208 also defined here
.
$
*MAT_DAMPER_NONLINEAR_VISCOUS
208      49
$
$
$$$$$$$$ Sections
$
$
$$$$ Shell Sections
$
*SECTION_SHELL
$   sid   elform      shrf      nip      propt   qr/irid   icomp
$     1     0 0.000E+00 0.000E+00 0.000E+00
$    t1     t2     t3     t4     nloc
1.000E-02 1.000E-02 1.000E-02 1.000E-02 0.000E+00
$
.
... shell sid's 2-21 also defined here
.
$
*SECTION_SHELL
$   sid   elform      shrf      nip      propt   qr/irid   icomp
$     22     0 0.000E+00 0.000E+00 0.000E+00
1.000E-02 1.000E-02 1.000E-02 1.000E-02 0.000E+00
$
$
$$$$ Spring-Damper Sections
$
*SECTION_SPRING-DAMPER
101      1 0.000E+00 0.000E+00 0.000E+00 0.000E+00

```

***MAT_SPRING**
Belted Dummy with Springs

```

0.000E+00 0.000E+00
$
.
... spring-damper sid's 102-207 also defined here
.
$
*SECTION_SPRING-DAMPER
208 1 0.000E+00 0.000E+00 0.000E+00 0.000E+00
0.000E+00 0.000E+00
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Nodes and Elements
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*NODE
$ node x y z tc rc
1-2.416931689E-01-3.286990896E-02 5.876007080E-01 0 0
2-2.475307435E-01-1.784761623E-02 5.820254087E-01 0 0
3-2.498186529E-01-1.089885016E-03 5.798402429E-01 0 0
.
... in total, 2043 nodes defined
.
2041-5.439429283E-01 2.696031034E-01 6.014695168E-01 0 0
2042-5.649484396E-01 2.777405977E-01 6.089934111E-01 0 0
2043-5.859540105E-01 2.858780622E-01 6.165173650E-01 5 0
$
$$$$ Shell Elements
$
*ELEMENT_SHELL
$ eid pid n1 n2 n3 n4
1 1 1 4 5 2
2 1 2 5 6 3
3 1 4 7 8 5
.
... in total, 1950 shells defined
.
1948 22 394 357 365 403
1949 22 403 365 367 404
1950 22 404 367 369 379
$
$$$$ Discrete Elements
$
*ELEMENT_DISCRETE
$ eid pid n1 n2 vid s pf offset
1 101 1 129 1 0.00000000E+00 1
2 102 1 129 2 0.00000000E+00 1
3 103 1 129 3 0.00000000E+00 1
.
... in total, 108 discrete elements defined
.
106 206 1505 1675 41 0.00000000E+00 1
107 207 1505 1675 42 0.00000000E+00 1
108 208 1505 1675 40 0.00000000E+00 1
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Segment sets for the contacts defined previously.
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$

```

***MAT_SPRING**
Belted Dummy with Springs

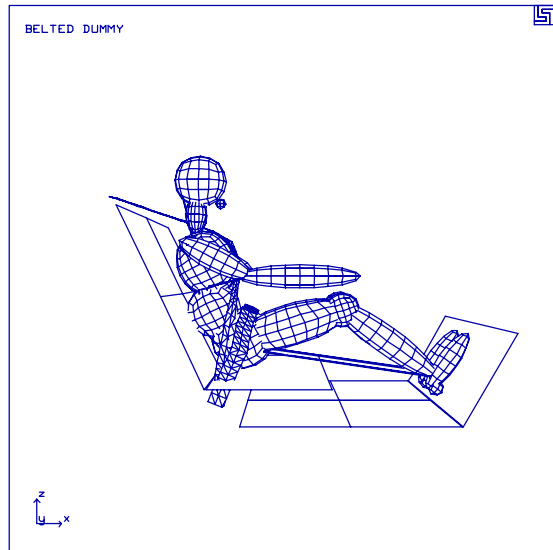
```
$
$.>...1.>...2.>...3.>...4.>...5.>...6.>...7.>...8
$
*SET_SEGMENT
$   sid      da1
    1         4
$   n1      n2      n3      n4
    1780    1783    1784    1781
    1783    1786    1787    1784
    1781    1784    1785    1782
    1784    1787    1788    1785
.
... in total, 22 segment sets defined for the contacts
.
$
*END
```

*MAT_SPRING

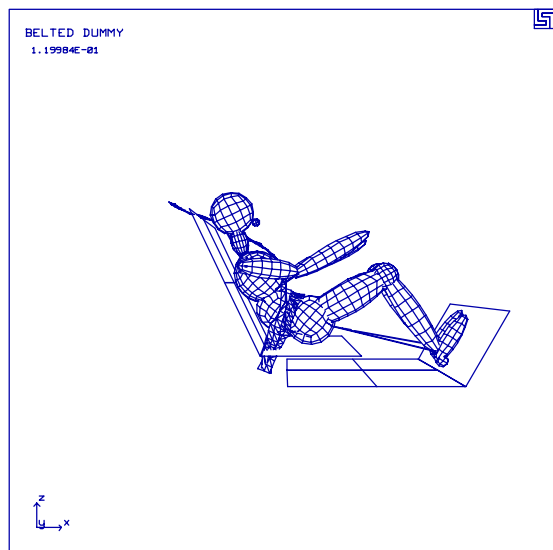
Belted Dummy with Springs

Results:

taurus g=d3plot
19
rx -90 center view



state 49
center
view



*MAT_TRANSVERSELY_ANISOTROPIC Rectangular Cup Drawing

LS-DYNA Manual Section: *MAT_TRANSVERSELY_ANISOTROPIC

Additional Sections:

*CONTACT_ONE_WAY_SURFACE_TO_SURFACE
*LOAD_SHELL_ELEMENT

Example: Rectangular Cup Drawing

Filename: mat_transversely_anisotropic.cup-draw.k

Description:

This problem includes three tools a punch, a holder and a die, and a blank. The blank is drawn by moving the punch downwards to form around the die. The blank uses the *MAT_TRANSVERSELY_ANISOTROPIC_ELASTIC_PLASTIC material model.

Model:

The *BOUNDARY_PRESCRIBED_MOTION_RIGID keyword is used to give the punch a prescribed velocity in the z-direction. All shells on the holder are given a pressure load to clamp down on the blank (*LOAD_SHELL_ELEMENT). One way surface to surface contact is defined between the major parts in the model. Because of symmetry, only 1/4 of the system is modeled.

Results:

A contour plot of the effective stress on the blank after drawing is shown.

*MAT_TRANSVERSELY_ANISOTROPIC

Rectangular Cup Drawing

List of LS-DYNA input deck:

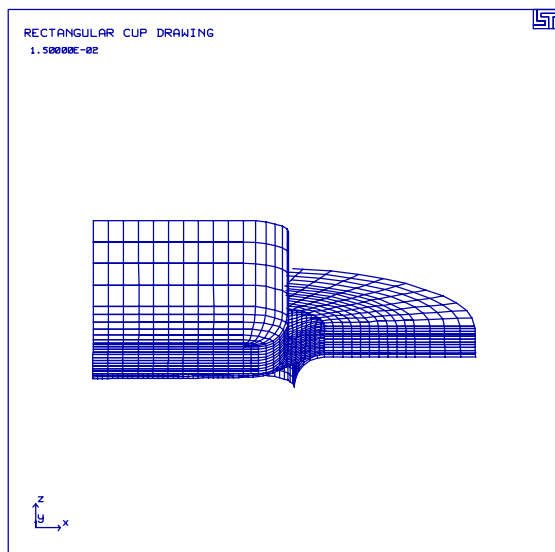
```
*KEYWORD
*TITLE
Rectangular Cup Drawing
$
$  LSTC Example
$
$  Last Modified: October 14, 1997
$
$$$  Original model received from Cray Research (John Gee)  - 7/19/95
$
$  The model consists of 4 parts:
$  1 - blank  (part that gets formed)
$  2 - die    (fixed part that forms the shape)
$  3 - holder (holds the blank from top)
$  4 - punch  (pushes down onto the blank)
$
$  The die, holder and punch are all rigid materials.
$
$  The blank is Mat #37
$    MAT_TRANSVERSELY_ANISOTROPIC_ELASTIC_PLASTIC
$
$  Units:   ton, mm, s, N, MPa, N-mm
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$. . . > . . . 1 . . . > . . . 2 . . . > . . . 3 . . . > . . . 4 . . . > . . . 5 . . . > . . . 6 . . . > . . . 7 . . . > . . . 8
$
*CONTROL_TERMINATION
$  endtim   endcyc     dtmin    endeng    endmas
$         .015
$
*CONTROL_CONTACT
$  slsfac   rwpnal     islchk   shlthk    penopt    thkchg    orien
$         0.1        0.0        1         2         0         2         2
$  usrstr   usrfac      nsbcs    interm    xopenen
$         0          0          0         0         4.0
$
*CONTROL_ENERGY
$  hgen     rwen      slnten   rylen
$         2         1         2         0
$
*CONTROL_OUTPUT
$  npopt    neecho    nrefup   iaccop    opifs     ipnint    ikedit
$         1         3         1         1         0.0
$
*CONTROL_SHELL
$  wrpang   itrlist   irnxx    istupd    theory    bwc       miter
$         20.0      1         -1        1         2         2
$
$
$
*DATABASE_BINARY_D3PLOT
$  dt       lcdt
$         0.002
$
*DATABASE_EXTENT_BINARY
$  neiph    neips     maxint   strflg    sigflg    epsflg    rtlflg    engflg
```


*MAT_TRANSVERSELY_ANISOTROPIC

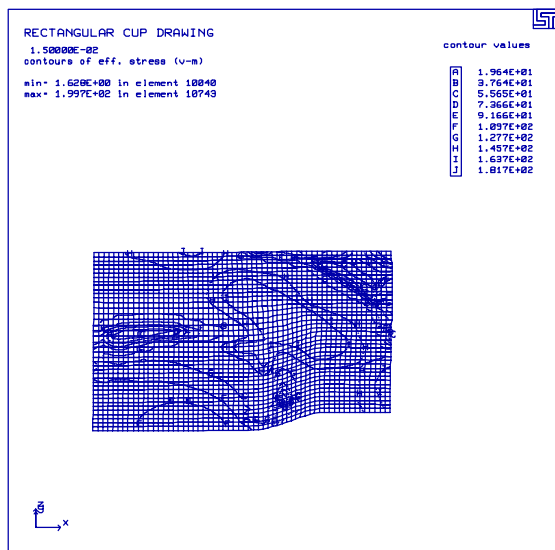
Rectangular Cup Drawing

Results:

taurus g=d3plot
angle 1 rx -90
state 20 view



m 1
numc 10 mono
rx 25 contour 9



***RIGIDWALL_GEOMETRIC_SPHERE_MOTION**

Rigid Wall Sphere Impacts a Plate

LS-DYNA Manual Section: *RIGIDWALL_GEOMETRIC_SPHERE_MOTION

Example: Rigid Wall Sphere Impacts a Plate

Filename: rigidwall_geometric_sphere.plate.k

Description:

A “Stonewall” - sphere impacts an elastic plate. (The sphere will not be shown in LS-TAURUS.)

Model:

The plate has an elastic material model with Belytschko-Tsay shell formulation. The plate is $40 \times 40 \times 2 \text{ mm}^3$. The sphere has a radius of 8 mm and its center is 9 mm above the plate. The sphere moves towards the plate with a prescribed displacement resulting in a velocity of velocity of 3 mm/second.

Input:

A spherical stonewall surface represents the true geometry of the ball. (*RIGIDWALL_GEOMETRIC_SPHERE_MOTION). The stonewall cards contain direction and load curve number defining the motion. All nodes of the plate are prevented from penetrating the sphere

Reference:

Schweizerhof, K. and Weimer, K.

***RIGIDWALL_GEOMETRIC_SPHERE_MOTION**
Rigid Wall Sphere Impacts a Plate

```

1        1        0.0       0.0       -1.0
$
$
*DEFINE_CURVE
$      lcid      sidr      scla      sclo      offa      offo
      1
$          abscissa          ordinate
           0.0              0.0
           0.0005           15.0
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*PART
$      pid      sid      mid      eosid      hgid      adpopt
plate  1        1        1
$
$
*MAT_ELASTIC
$      mid      ro      e      pr      da      db      k
      1  2.00e-08  100000.  0.300
$
$
*SECTION_SHELL
$      sid      elform      shrf      nip      propt      qr/irid      icomp
      1              0.83333      2.0      3.0
$      t1      t2      t3      t4      nloc
      2.0      2.0      2.0      2.0
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Define Nodes and Elements
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Nodes on the outside edges of the plate are constrained in z-translation.
$
*NODE
$      node      x      y      z      tc      rc
      1  0.000000E+00  0.000000E+00  0.000000E+00  3      0
      2  5.000000E+00  0.000000E+00  0.000000E+00  3      0
      3  1.000000E+01  0.000000E+00  0.000000E+00  3      0
      .
      ... in total, 81 nodes defined
      .
      79  3.000000E+01  4.000000E+01  0.000000E+00  3      0
      80  3.500000E+01  4.000000E+01  0.000000E+00  3      0
      81  4.000000E+01  4.000000E+01  0.000000E+00  3      0
$
$$$$$  Shell Elements
$
*ELEMENT_SHELL
$      eid      pid      n1      n2      n3      n4
      1        1        1        2        11       10
      2        1        2        3        12       11
      3        1        3        4        13       12

```

***RIGIDWALL_GEOMETRIC_SPHERE_MOTION**

Rigid Wall Sphere Impacts a Plate

.
... in total, 64 shells defined

62	1	69	70	79	78
63	1	70	71	80	79
64	1	71	72	81	80

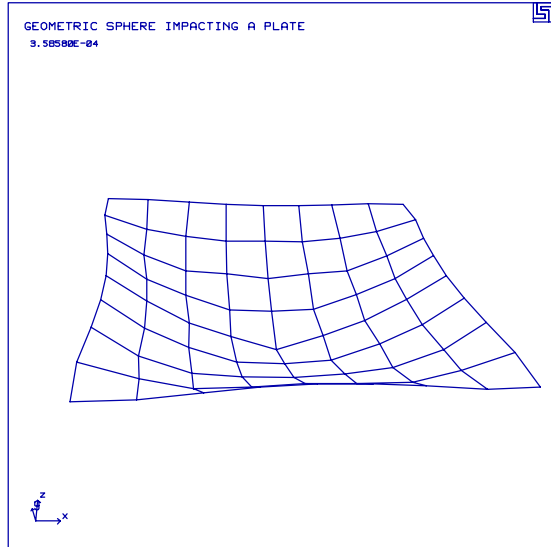
\$.
*END

*RIGIDWALL_GEOMETRIC_SPHERE_MOTION

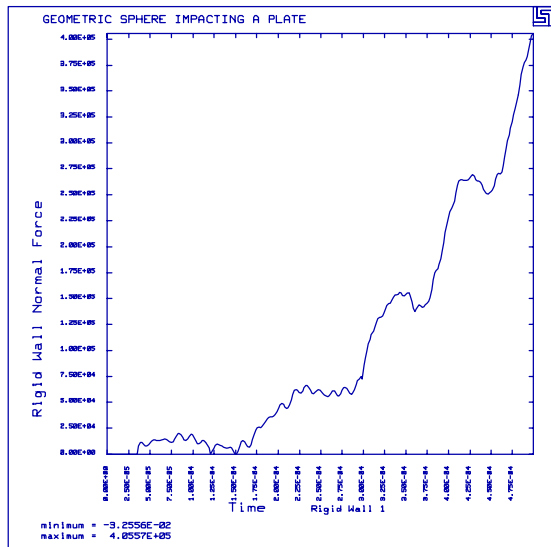
Rigid Wall Sphere Impacts a Plate

Results:

taurus g=d3plot
19
rx -60 ry 10 state 19 view



phs3
rwforc
normal



***RIGIDWALL_GEOMETRIC_SPHERE_MOTION**

Rigid Wall Sphere Impacts a Plate

LS-DYNA Manual Section: *RIGIDWALL_PLANAR

Additional Sections:

*INITIAL_VELOCITY_NODE

Example: Rotating Shell Strikes Rigid Wall

Filename: rigidwall_planar.shell.k

Description:

A rotating shell element strikes and rebounds from a rigid wall surface. The plate is modeled with shell elements for viewing in LS-TAURUS. This does not affect the calculation.

Model:

The shell element has an elastic material model with Belytschko-Tsay shell formulation. The plate measures $10 \times 10 \times 2 \text{ mm}^3$. The plate has an initial velocity of 100,000 mm/second in negative z-direction and an initial angular velocity of 100,000 radians/second about the y-axis. The rigid surface is modeled by an infinite smooth stonewall surface.

Input:

Nodes requiring initial velocity are specified with *INITIAL_VELOCITY_NODE. The location of the “Stonewall” is in the x-y plane with $z=0$ (*RIGIDWALL_PLANAR). The 4 nodes belonging to the shell element are slave nodes in the stonewall definition. The velocity components of the slave nodes in the normal direction to the stonewall are reset to zero at the moment of impact.

Reference:

Schweizerhof, K. and Weimer, K.

*RIGIDWALL_PLANAR

Rotating Shell Strikes Rigid Wall

List of LS-DYNA input deck:

```

*KEYWORD
*TITLE
STONEWALL SURFACE
$
$  LSTC Example
$
$  Last Modified: September 23, 1997
$
$  Units: ton, mm, s, N, MPa, N-mm
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1....>...2....>...3....>...4....>...5....>...6....>...7....>...8
$
*CONTROL_TERMINATION
$  endtim  endcyc  dtmin  endneg  endmas
2.000E-04
$
*CONTROL_ENERGY
$    hgen  rwen  slnten  rylen
        2      2
$
$
$
*DATABASE_BINARY_D3PLOT
$    dt    lcdt
1.000E-05
$
*DATABASE_BINARY_D3THDT
$    dt    lcdt
2.000E-03
$
$
*DATABASE_GLSTAT
$    dt
4.0e-06
$
$
*DATABASE_NODOUT
$    dt
4.0e-06
$
$
*DATABASE_HISTORY_NODE
$    i      i      i      i      i      i      i      i      i
$    id1    id2    id3    id4    id5    id6    id7    id8
        12     13     101
$
$
*DATABASE_RWFORC
$    dt
4.0e-06
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Rigidwalls
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1....>...2....>...3....>...4....>...5....>...6....>...7....>...8
$
$

```

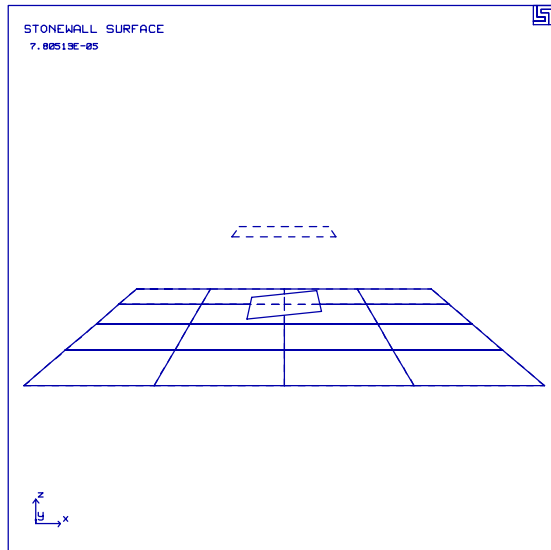
***RIGIDWALL_PLANAR**
Rotating Shell Strikes Rigid Wall

```
$$$$ The nodes in set 1 (nodes of the moving shell) are prevented from
$$$$ penetrating the rigidwall.
$
*RIGIDWALL_PLANAR
$      nsid      nsidex      boxid
$        1
$
$
$      xt      yt      zt      xh      yh      zh      fric
$
$      20.000   20.000   0.000 20.00000 20.00000 100.000
$
$
$
*SET_NODE_LIST
$      sid
$        1
$      nid1      nid2      nid3      nid4      nid5      nid6      nid7      nid8
$        101      102      103      104
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Initial Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
$$$$ Nodes of the moving shell are given an initial tran and rot velocity.
$
*INITIAL_VELOCITY_NODE
$      nid      vx      vy      vz      vxe      vye      vze
$        101 0.000E+00 0.000E+00-1.000E+05 0.000E+00 1.000E+05 0.000E+00
$        102 0.000E+00 0.000E+00-1.000E+05 0.000E+00 1.000E+05 0.000E+00
$        103 0.000E+00 0.000E+00-1.000E+05 0.000E+00 1.000E+05 0.000E+00
$        104 0.000E+00 0.000E+00-1.000E+05 0.000E+00 1.000E+05 0.000E+00
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*PART
$      pid      sid      mid      eosid      hgid      adpopt
wall
$         1         1         1
moving-shell
$         2         2         2
$
$
$
*MAT_ELASTIC
$      mid      ro      e      pr      da      db      k
$         1 1.000E-08 1.000E+05 3.000E-01
$
*MAT_ELASTIC
$      mid      ro      e      pr      da      db      k
$         2 1.000E-08 1.000E+05 3.000E-01
$
$
$
*SECTION_SHELL
$      sid      elform      shrf      nip      propt      qr/irid      icomp
```

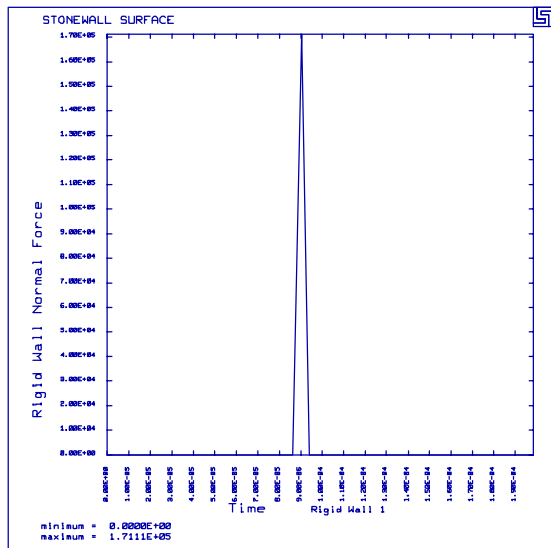

*RIGIDWALL_PLANAR Rotating Shell Strikes Rigid Wall

Results:

taurus g=d3plot
19
udg 1 state 9 rx -80 view



phs3
rwforc
normal



***RIGIDWALL_PLANAR**

Rotating Shell Strikes Rigid Wall

LS-DYNA Manual Section: *RIGIDWALL_PLANAR_FORCES

Example: Cube Rebounding

Filename: rigidwall_planar.cube.k

Description:

A cube impacts and rebounds from a rigid plate (“Stonewall”). The plate is modeled with shell elements for viewing in LS-TAURUS.

Model:

The cube measures $10 \times 10 \times 10 \text{ mm}^3$ and is 10 mm above the rigid plate. It has 8 brick elements with elastic material properties. The initial velocity of the cube is 100,000 mm/second. The plate is an infinite “Stonewall” - surface

Input:

The box option defines the nodes with the initial velocity (*DEFINE_BOX, *INITIAL_VELOCITY). The location of the “Stonewall” is at $z=0$ (*RIGIDWALL_PLANAR_FORCES). The nine nodes on the lower side of the cube are slave nodes to the “Stonewall” definition. The soft option of the rigidwall is used, which means that the slave nodes will come to stop within 10 time steps of initial contact with the rigidwall.

Reference:

Schweizerhof, K. and Weimer, K.

*RIGIDWALL_PLANAR_FORCES

Cube Rebounding

```

$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*RIGIDWALL_PLANAR_FORCES
$      nsid      nsidex      boxid
$            1          0          0
$
$      xt        yt        zt      xh      yh      zh      fric
$      20.0      20.0      0.0     20.0     20.0     100.0    0.000
$
$      soft      ssid      nid1      nid2      nid3      nid4
$      10        0        1        4        13        16
$
$
$
*SET_NODE_LIST
$      sid
$            1
$      nid1      nid2      nid3      nid4      nid5      nid6      nid7      nid8
$      201      202      203      204      205      206      207      208
$      209
$
$
$$$$ Initial Conditions
$
$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
$$$$ All nodes located within box 1 are given an initial velocity.
$
*INITIAL_VELOCITY
$      nsid      nsidex      boxid
$                               1
$      vx        vy        vz
$      0.0        0.0 -100000.0
$
$
*DEFINE_BOX
$      boxid      xmm      xmx      ymn      ymx      zmn      zmx
$            1      14.9      25.1      14.9      25.1      9.0      21.0
$
$
$$$$ Define Parts and Materials
$
$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*PART
$      pid      sid      mid      eosid      hgid      adpopt
wall-display
$      1        1        1
cube
$      2        2        2        0        0        0
$
$
$
*MAT_ELASTIC
$      mid      ro      e      pr      da      db
$      1      2.00e-8 100000.0 0.300
$
*MAT_ELASTIC

```

*RIGIDWALL_PLANAR_FORCES

Cube Rebounding

```

$      mid      ro      e      pr      da      db
$      2      1.00e-8 100000.0 0.300
$
$
$
*SECTION_SHELL
$      sid      elform      shrf      nip      propt      qr/irid      icomp
$      1      0.83333      2.0      3.0
$      t1      t2      t3      t4      nloc
$      2.0      2.0      2.0      2.0
$
*SECTION_SOLID
$      sid      elform
$      2
$
$$$$$ Define Nodes and Elements
$
$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*NODE
$      node      x      y      z      tc      rc
$      1      5.000000E+00 5.000000E+00 0.000000E+00 7 0
$      4      3.500000E+01 5.000000E+00 0.000000E+00 7 0
$      13     3.500000E+01 3.500000E+01 0.000000E+00 0 0
$
$      ... in total, 31 nodes defined
$
$      201     1.500000E+01 1.500000E+01 1.000000E+01 0 0
$      225     1.500000E+01 2.500000E+01 2.000000E+01 0 0
$      226     2.000000E+01 2.500000E+01 2.000000E+01 0 0
$      227     2.500000E+01 2.500000E+01 2.000000E+01 0 0
$
$$$$$ Shell Elements - For Display of the Rigidwall
$
*ELEMENT_SHELL
$      eid      pid      n1      n2      n3      n4
$      1      1      1      4      13     16
$
$$$$$ Solid Elements
$
*ELEMENT_SOLID
$      eid      pid      n1      n2      n3      n4      n5      n6      n7      n8
$      101     2      201     202     205     204     210     211     214     213
$      102     2      202     203     206     205     211     212     215     214
$      103     2      204     205     208     207     213     214     217     216
$      104     2      205     206     209     208     214     215     218     217
$      105     2      210     211     214     213     219     220     223     222
$      106     2      211     212     215     214     220     221     224     223
$      107     2      213     214     217     216     222     223     226     225
$      108     2      214     215     218     217     223     224     227     226
$
*END

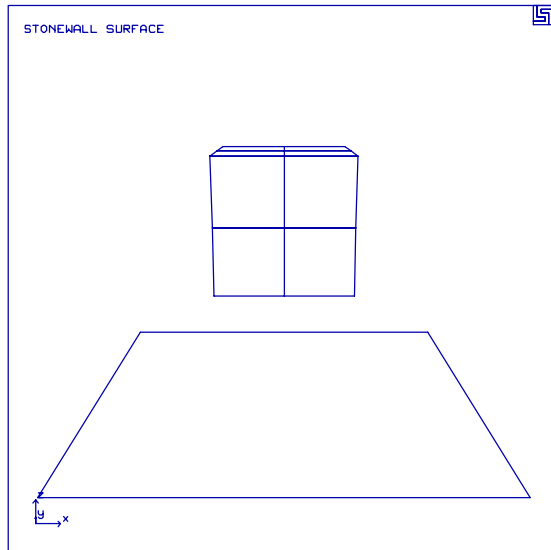
```

*RIGIDWALL_PLANAR_FORCES

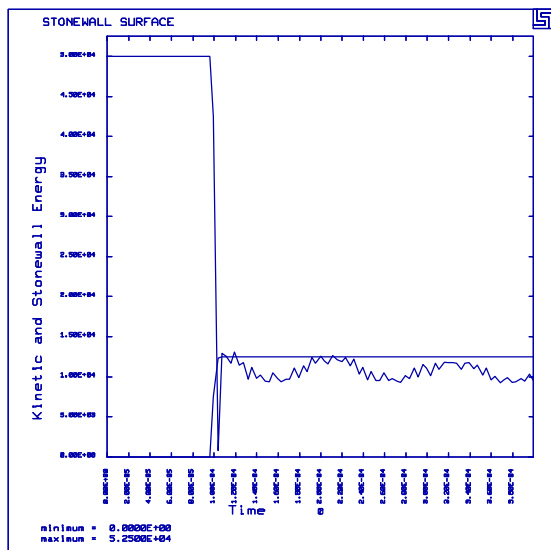
Cube Rebounding

Results:

taurus g=d3plot
19
rx -80 view



phs3 glstat
otxt Kinetic and Stonewall Energy
oset 0 5.25e4 kinetic over stonewall



***RIGIDWALL_PLANAR_FORCES**

Cube Rebounding

LS-DYNA Manual Section: *RIGIDWALL_PLANAR_MOVING

Additional Sections:

*CONTACT_AUTOMATIC_SINGLE_SURFACE

Example: Symmetric Crush Tube

Filename: rigidwall_planar.symtube.k

Description:

A tube is crushed using a planar, moving rigid wall.

Model:

Because of symmetry , only 1/4 of the system is modeled. Automatic single surface contact is defined to prevent penetrations as the tube folds on itself. The bottom nodes of the tube are fixed using SPC's. The top of the tube is hit by a rigid wall that is defined with a mass of 800 kg and an initial velocity of 8.94 mm/ms in the negative z-direction. The friction coefficient on the wall is 1.0, this means that the nodes are prevented from sliding along the plane of the wall. An extra node is defined and associated with the rigid wall so that the walls velocity and displacement can be tracked in the ascii output file nodout (node id 99999).

Results:

The tubes crush and the wall forces from the ascii output file rwforc are shown. The force-deflection of the crush tube can be obtained by using the force data from rwforc and the displacement data from nodout.

***RIGIDWALL_PLANAR_MOVING**
Symmetric Crush Tube

```

$
*DATABASE_HISTORY_NODE
$   id1      id2      id3      id4      id5      id6      id7      id8
     99999    414      486
$
*DATABASE_RWFORC
$   dt
     0.1
$
*DATABASE_SLEOUT
$   dt
     0.1
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Contacts - Sliding Interfaces
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1.>...2.>...3.>...4.>...5.>...6.>...7.>...8
$
*CONTACT_AUTOMATIC_SINGLE_SURFACE
$   ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
     0
$   Equating ssid to zero means that all segments are included in the contact
$
$   fs        fd        dc        vc        vdc        penchk      bt        dt
     0.08     0.08
$
$   sfs       sfm       sst       mst       sfst       sfmt        fsf       vsf
$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Rigidwalls
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1.>...2.>...3.>...4.>...5.>...6.>...7.>...8
$
*RIGIDWALL_PLANAR_MOVING_FORCES
$   nsid      nsidex      boxid
     0         0         0
$
$   xt        yt        zt        xh        yh        zh        fric
     0.0      0.0      274.0    0.0      0.0      0.0      1.0
$
$   sw mass   sw vel
     800.000  8.94000
$
$   soft      ssid      node1      node2      node3      node4
     0         0        99999
$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1.>...2.>...3.>...4.>...5.>...6.>...7.>...8
$
*PART

```


***RIGIDWALL_PLANAR_MOVING**
Symmetric Crush Tube

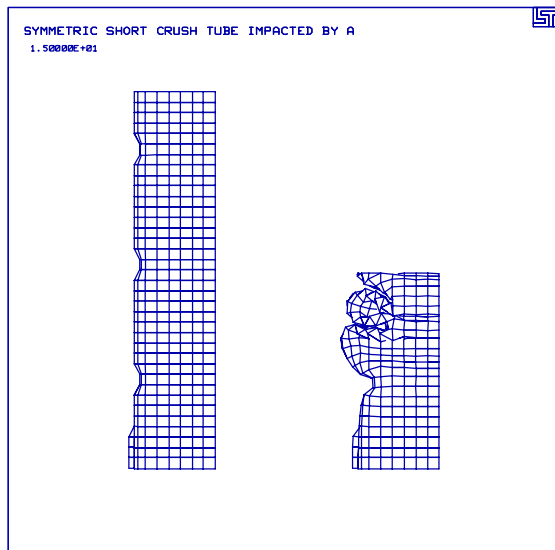
```
715 -5.80000000E+01 -2.40000000E+01 2.724830000E+02 0 0
716 -5.80000000E+01 -3.20000000E+01 2.724830000E+02 0 0
$
$$$$$$$$ Shell Elements
$
*ELEMENT_SHELL
$  eid      pid      n1      n2      n3      n4
   752      1      547      552      553      553
   753      1      553      548      547      547
     1      1      1      2      9      8
     2      1      2      3      10     9
     .
     ... in total, 467 shells defined
     .
   640      1      710      711      716      715
   641      1      711      485      487      716
$
*END
```

*RIGIDWALL_PLANAR_MOVING

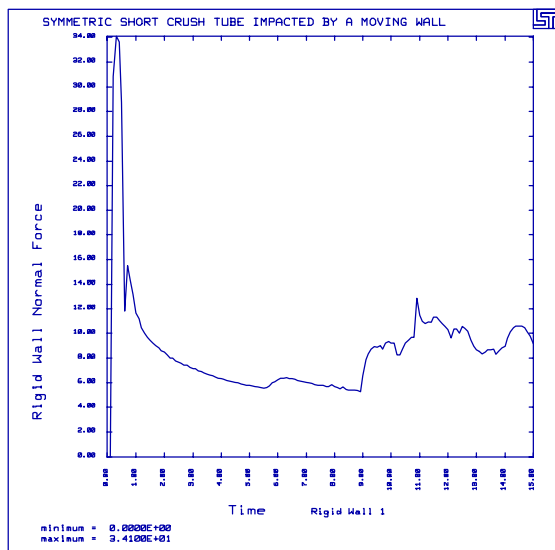
Symmetric Crush Tube

Results:

taurus g=d3plot
angle 1 rx -90 xtrans -80 view
xtrans 160 state 16 over view



phs3
rwforc
oscl -1 normal



LS-DYNA Manual Section: *SECTION_SHELL

Additional Sections:

*CONSTRAINED_SPOTWELD
*LOAD_NODE_POINT

Example: Fuse Plate in Tension Exhibits Hourglassing

Filename: section_shell.hourglassing.k

Description:

A fuse plate is used to connect a cut in a wide flange beam. The beam is loaded at an end, putting the fuse plate in tension. In this loading condition, the fuse plate exhibits a great deal of hourglassing.

Model:

The fuse plate and beam are constructed with shell elements and a piecewise linear plasticity material model with failure. The fuse plate is connected to the beam using spot welds (*CONSTRAINED_SPOTWELD). One end of the beam is fixed with SPC's, while the other end has several nodal point loads (*BOUNDARY_SPC_NODE, *LOAD_NODE_POINT). Multiple point loads are used to better distribute the input loads.

Results:

One look at the figures explains why it's called "hourglassing". To fix the hourglassing problem the fuse plate could be re-meshed or a fully integrated shell element formulation could be used.

*SECTION_SHELL

Fuse Plate in Tension Exhibits Hourglassing

```

      1      1      1
postweb
      2      2      1
fuseplat
      3      3      1
$
$
$$$$ Materials
$
$
*MAT_PIECEWISE_LINEAR_PLASTICITY
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$      mid      ro      e      pr      sigy      etan      eppf      tdel
      1 0.783E-05 2.000E+02      0.3 2.070E-01      7.500E-01
$ Cowper/Symonds Strain Rate Parameters
$      c      p      lcss      lcsr
      40      5
$ Plastic stress/strain curve
      0.000E+00 8.000E-02 1.600E-01 4.000E-01 9.900E+01
      2.070E-01 2.500E-01 2.750E-01 2.899E-01 3.000E-01
$
$
$$$$ Sections
$
*SECTION_SHELL
$      sid      elform      shrf      nip      propt      qr/irid      icode
      1      6
$      t1      t2      t3      t4      nloc
5.4600E+00 5.460E+00 5.460E+00 5.460E+00
$
*SECTION_SHELL
$      sid      elform      shrf      nip      propt      qr/irid      icode
      2      6
$      t1      t2      t3      t4      nloc
4.3200E+00 4.320E+00 4.320E+00 4.320E+00
$
$
*SECTION_SHELL
$      sid      elform      shrf      nip      propt      qr/irid      icode
      3      2
$      3      6
$      t1      t2      t3      t4      nloc
4.7625E+00 4.762E+00 4.762E+00 4.762E+00
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Nodes and Elements
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*NODE
$      node      x      y      z      tc      rc
      1 0.000000000E+00 7.500000000E+01 2.337080000E+03      0      0
      2 8.750000000E+01 5.000000000E+01 2.360630000E+03      0      0
      .
      ... in total, 522 nodes defined
      .
      675 0.000000000E+00 2.500000000E+01 2.286845000E+03      0      0
      676 0.000000000E+00 7.500000000E+01 2.286845000E+03      0      0
$
```

***SECTION_SHELL**
Fuse Plate in Tension Exhibits Hourglassing

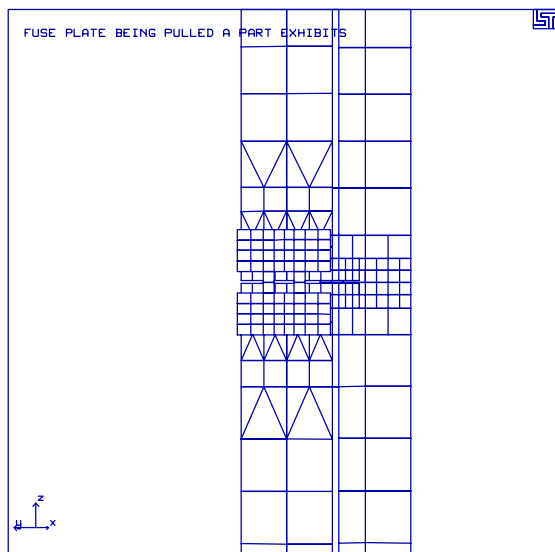
```
$$$$$$$ Shell Elements
$
*ELEMENT_SHELL
$   eid      pid      n1      n2      n3      n4
   487        1      647      123      501      501
   488        1      647      501      653      653
   .
   ... in total, 436 shells defined
   .
   387        3      499      496      289      497
   388        3      422      499      497      287
$
*END
```

*SECTION_SHELL

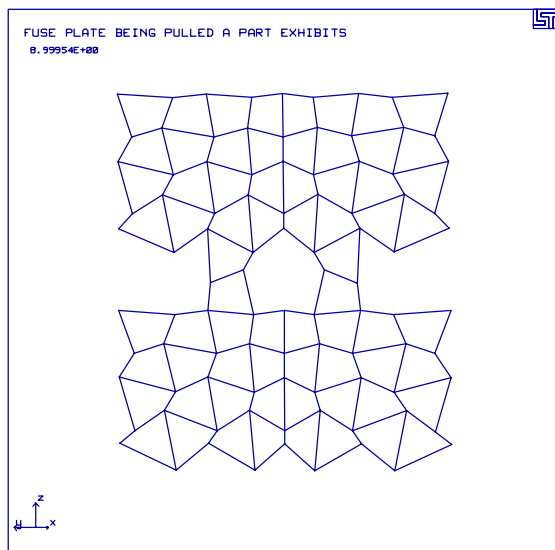
Fuse Plate in Tension Exhibits Hourglassing

Results:

taurus g=d3plot
angle 1 rx -90 ry 60 m 3 center
zmax 50000 dist 30000 dam view



s 10
m 3
center view



LS-DYNA Manual Section: *SECTION_SOLID

Additional Sections:

*CONTACT_ERODING_SINGLE_SURFACE
*INITIAL_VELOCITY_GENERATION

Example: Breaking Post Exhibits Hourglassing

Filename: section_solid.hourglassing.k

Description:

A rigid beam strikes a post near the top of the post. There is hole cut out of the lower portion of the post to reduce its' section modulus and thus, allow it to snap-off easier. In the first model, the post begins to break, but hourglassing starts to dominate the solution and the post does not completely snap.

In the second model, a fully integrated solid formulation is used for the post, causing the post to snap-off as desired.

Model:

The beam is constructed with rigid shell elements. An initial velocity is given to the beam using the *INITIAL_VELOCITY_GENERATION keyword. The post is constructed with solid elements using a piecewise linear plasticity material model with failure. Single point constraints (SPC's) are placed on the bottom of the post. Eroding single surface contact is required in order for the contact to behave properly while the post snaps in two (*CONTACT_ERODING_SINGLE_SURFACE).

Results:

The first model results are significantly different than the second model due to hourglassing.

***SECTION_SOLID**
Breaking Post Exhibits Hourglassing

```
$      dt
      0.10
$
*DATABASE_HISTORY_NODE
$      id1      id2      id3      id4      id5      id6      id7      id8
      758
$
*DATABASE_RBDOUT
$      dt
      0.10
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Contacts - Sliding Interfaces
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
*CONTACT_ERODING_SINGLE_SURFACE
$      ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
      0
$      fs      fd      dc      vc      vdc      penchk      bt      dt
$      sfs      sfm      sst      mst      sfst      sfmt      fsf      vsf
$      isym      erosop      iadj
          1      1
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Initial and Boundary Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1.>...2.>...3.>...4.>...5.>...6.>...7.>...8
$
$$$$ The beam (part 3) is given an initial velocity towards the post.
$
*INITIAL_VELOCITY_GENERATION
$      sid      styp      omega      vx      vy      vz
      3      2      27.8      0.0      0.0
$      xc      yc      zc      nx      ny      nz      phase
$
$$$$ Fix the bottom nodes of the post.
$
*BOUNDARY_SPC_NODE
$.>...1.>...2.>...3.>...4.>...5.>...6.>...7.>...8
$      nid cid x y z rx ry rz
      163,  0,1,1,1, 1, 1, 1
      166,  0,1,1,1, 1, 1, 1
      .
      ... in total, 28 SPC's defined
      .
      645,  0,1,1,1, 1, 1, 1
      648,  0,1,1,1, 1, 1, 1
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
```

***SECTION_SOLID**

Breaking Post Exhibits Hourglassing

\$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8

\$
 \$\$\$ Part 3 shell: beam
 \$
 \$\$\$ Part 4 solid: lower_post
 \$
 \$\$\$ Part 5 solid: upper_post
 \$
 \$

*PART
 \$ pid sid mid eosid hgid grav adpopt
 bumper
 3 1 1
 lower_post
 4 2 2
 upper_post
 5 2 3
 \$

\$\$\$\$ Materials

\$\$ Bumper - Rigid, constrained to translate only in the x-direction

*MAT_RIGID
 \$ mid ro e pr n couple m alias
 1 0.143E-02 200.0 0.33
 \$
 \$ cmo con1 con2
 1.0 5 7
 \$
 \$ lco/a1 a2 a3 v1 v2 v3
 \$

\$\$ Post - the lower portion is softer and fails sooner than the upper portion

*MAT_PIECEWISE_LINEAR_PLASTICITY
 \$ mid ro e pr sigy etan eppf tdel
 2 0.499E-06 11.37 0.32 0.0468 0.11
 \$
 \$ c p lcss lcsr
 \$ Plastic stress/strain curve
 0.0000 0.2500
 0.0468 0.0470
 \$

*MAT_PIECEWISE_LINEAR_PLASTICITY
 \$ mid ro e pr sigy etan eppf tdel
 3 0.499E-06 110.37 0.32 0.0468 0.25
 \$
 \$ c p lcss lcsr
 \$ Plastic stress/strain curve
 0.0000 0.2500
 0.0468 0.0470
 \$

\$\$\$\$ Sections

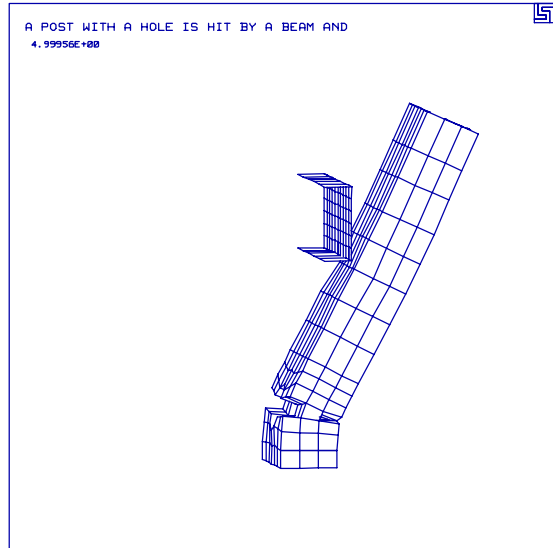
*SECTION_SHELL
 \$ sid elform shrf nip propt qr/irid icomp

*SECTION_SOLID

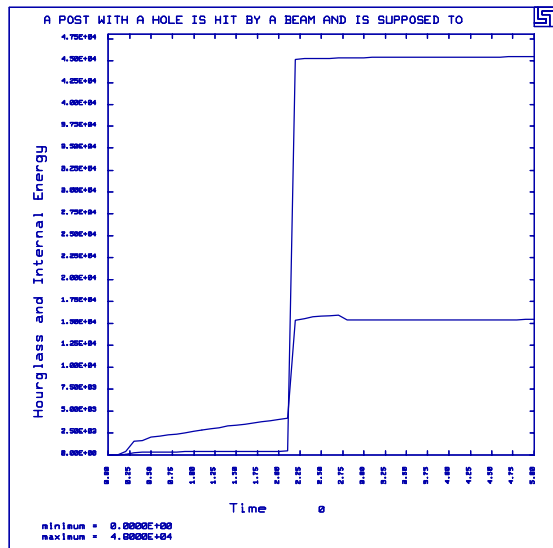
Breaking Post Exhibits Hourglassing

Results:

taurus g=d3plot
angle 1 rx -90 state 11
ry 10 rx 5 view



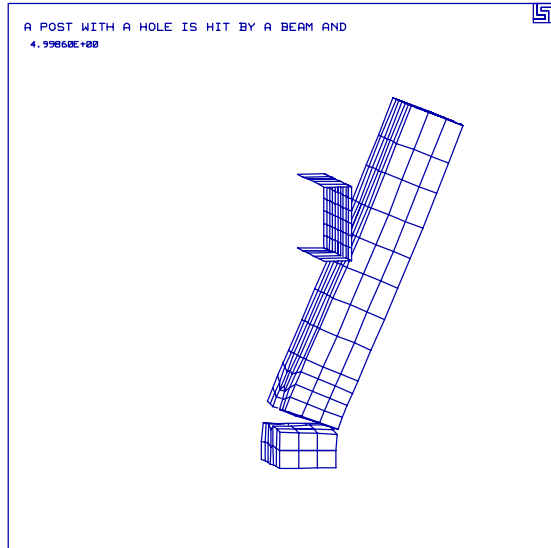
phs3 glstat
otxt Hourglass and Internal Energy
oset 0 4.8e4 hour over internal



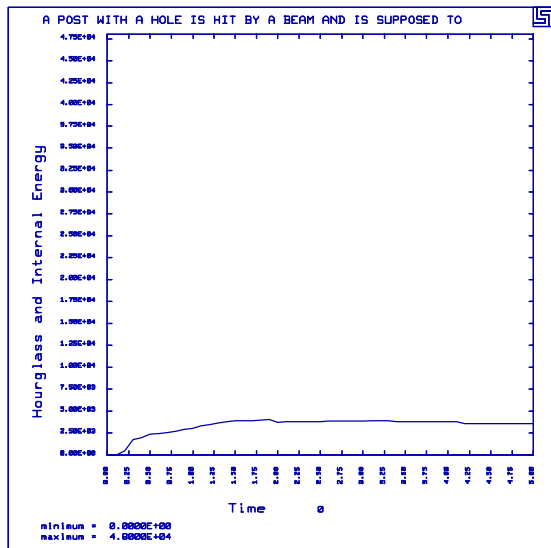
***SECTION_SOLID**
Breaking Post Exhibits Hourglassing

Results - No Hourglassing:

taurus g=d3plot
angle 1 rx -90 state 11
ry 10 rx 5 view



phs3 glstat
otxt Hourglass and Internal Energy
oset 0 4.8e4 hour over internal



***SECTION_SOLID**

Breaking Post Exhibits Hourglassing

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